Evaluation of a Proposed Gas Sampling Method Performance Verification Test Protocol

FINAL REPORT

Prepared by:

D. L. George R. A. Hart M. Nored

SOUTHWEST RESEARCH INSTITUTE®
Mechanical and Fluids Engineering Division
6220 Culebra Road
San Antonio, Texas, USA 78238-5166

Prepared for:

United States Minerals Management Service Engineering and Research 381 Elden Street, MS-4021 Herndon, VA 20240

Sharon Buffington, Project Manager

Disclaimer

This report was prepared by Southwest Research Institute (SwRI®) as an account of contracted work sponsored by the United States Minerals Management Service (MMS). Neither SwRI, MMS, members of these organizations, nor any person acting on their behalf:

- a. Makes any warranty or representation, express or implied, with respect to the accuracy, completeness, or usefulness of the information contained in this report, or that the use of any information, apparatus, methods, or process disclosed in this report may not infringe upon privately owned rights; or
- b. Assumes any liability with respect to the use of, or for damages resulting from the use of, any information, apparatus, method, or process disclosed in this report.

References to trade names or specific commercial products, commodities, or services in this report does not represent or constitute an endorsement, recommendation, or favoring by SwRI or MMS of the specific commercial product, commodity, or service.

TABLE OF CONTENTS

		Page
LIST	OF FIGURES	iv
LIST	OF TABLES	vi
1.0	INTRODUCTION	1
2.0	TEST PROTOCOL AND SAMPLING METHODS	3
2.1	PERFORMANCE VERIFICATION TEST PROTOCOL	
2.2		
	2.2.1 Established Sampling Methods Tested Using the Protocol	
	2.2.2 Proposed New Sampling Methods Tested Using the Protocol	
2	2.2.3 Sampling Methods Considered but Not Tested	
3.0	SAMPLING TESTS	7
3.1	VERIFICATION TESTS PERFORMED UNDER OPTIMUM CONDITIONS	7
3	8.1.1 Facility and Equipment	
3	3.1.2 Test Conditions	
_	3.1.3 Results	
3.2	VERIFICATION TESTS PERFORMED UNDER ADVERSE CONDITIONS	
_	3.2.1 Facility and Equipment	
_	3.2.2 Test Conditions	
_	3.2.3 Results	
_	3.2.4 Test Conditions – Repeat Tests	
3.3	3.2.5 Results – Repeat Tests	
3.3		
4.0	CONCLUSIONS	31
5.0	REFERENCES	33
APPI	ENDIX A PROPOSED PERFORMANCE VERIFICATION TEST P	ROTOCOL 35
APPI	ENDIX B PROCEDURES FOR NEW SAMPLING METHODS	41
APPI	ENDIX C GC SETUP AND CALIBRATION RESULTS	49
C. 1	LABORATORY INSPECTION CHECKLIST	51
	2 GC CALIBRATIONS	
	C.2.1 MRF GC	
	C.2.2 Powder Wash GC	
(C.2.3 Powder Wash GC - Repeat Tests	63
APPI	ENDIX D DETAILED TEST RESULTS	65

LIST OF FIGURES

		Page
Figure 1.	Schematic of the MRF test section showing the piping arrangement and spot sampling locations.	7
Figure 2.	MRF test section piping configured for the sampling tests. The schematic for this setup is shown in Figure 1	8
Figure 3.	Sampling equipment used in tests of the Controlled Rate Purge method at the MRF. Bottom left, pigtail and end valve; bottom right, sample probes with isolation valve and pressure gauge connection. The scale on the tape measure is in inches.	9
Figure 4.	Dew scope connected to the MRF test section for determination of the gas stream HCDP.	10
Figure 5.	Stream analyses from 10:40 am and 3:25 pm on June 18, illustrating the drift that was observed in the portable GC during the MRF tests	11
Figure 6.	Gas velocity and pressure in the loop during the sampling tests conducted at the MRF. Vertical dashed lines show intervals during which samples were drawn using the various methods. Flow was in a 6" diameter Schedule 80 pipe	12
Figure 7.	Equipment and gas temperatures during the sampling tests conducted at the MRF. Black vertical lines with long dashes indicate intervals during which samples were drawn using the various methods. Red vertical lines with shorter dashed lines indicate times when GC analyses of the flowing stream were obtained.	13
Figure 8.	Pipeline and sampling locations at the Powder Wash field site	16
	Configuration of the equipment used for collecting samples at the Powder Wash field site. Left, Controlled Rate Purge; center, Fill-and-Empty; right, High-Pressure Helium Displacement	17
Figure 10	. Configuration of the equipment used for collecting samples with the Pitot and Bypass method at the Powder Wash field site	18
Figure 11	. Sampling probes used for the Powder Wash tests. Left, curved probes for the Pitot and Bypass method; right, example of a straight probe used for the other sampling methods.	18
Figure 12	. Long-term trends in flowing stream heating value and nitrogen content around the time of the sampling tests conducted in November at the Powder Wash field site.	20

Figure 13.	Gas velocity and pressure in the pipeline during the sampling tests conducted in November at the Powder Wash field site. Vertical dashed lines show intervals during which samples were taken using the various sampling methods. Flow was in an 8" diameter pipe	21
Figure 14.	Typical sampling arrangement at the Powder Wash field site showing which portions of the system were not insulated during the November tests. The attached lines and valves were insulated during the December retests.	21
Figure 15.	Equipment and gas temperatures during the sampling tests conducted in November 2003 at the Powder Wash field site. Black vertical lines with long dashes indicate intervals during which samples were drawn using the various methods. Red vertical lines with shorter dashed lines indicate times when GC analyses of the flowing stream were obtained	22
Figure 16.	Long-term trends in stream heating value and nitrogen content around the time of the sampling tests conducted in December at the Powder Wash field site.	25
Figure 17.	Flowing gas velocity and line pressure in the pipeline during the sampling tests conducted in December at the Powder Wash field site. Vertical dashed lines show intervals during which samples were taken by the various methods. Flow was in an 8" diameter pipe.	26
Figure 18.	Equipment and gas temperatures during the sampling tests conducted in December 2003 at the Powder Wash field site. Black vertical lines with long dashes indicate intervals during which samples were drawn using the various methods. Red vertical lines with shorter dashed lines indicate times when GC analyses of the flowing stream were obtained	27
Figure C-1	. Dew point curve for gas used to calibrate the Daniel 2350 GC at the MRF. Curve computed from SRK equation of state	59
Figure C-2	2. Fidelity plot for column A of the MRF Daniel 2350 GC. June 2003 calibration runs on Scott gas #XL002396.	59
Figure C-3	Fidelity plot for column B of the MRF Daniel 2350 GC. June 2003 calibration runs on Scott gas #XL002396.	60
Figure C-4	Dew point curves for gases used to calibrate the Varian CP-4900 GC at the Powder Wash site. Curves computed from SRK equation of state	61
Figure C-5	5. Fidelity plot for column A of the Varian CP-4900 GC at the Powder Wash site. November 11 calibration run on DCG gas #22933AW	61

Figure C-6.	Fidelity plot for column B of the Varian CP-4900 GC at the Powder Wash site. November 11 calibration run on DCG gas #22933AW	2
Figure C-7.	Fidelity plot for column A of the Varian CP-4900 GC at the Powder Wash site. November 12 calibration run on Scott gas #ALM051559	2
Figure C-8.	Fidelity plot for column B of the Varian CP-4900 GC at the Powder Wash site. November 12 calibration run on Scott gas #ALM051559	3
Figure C-9.	Fidelity plot for column A of the Varian CP-4900 GC at the Powder Wash site. December 18 calibration run on DCG gas #22933AW	4
Figure C-10	. Fidelity plot for column B of the Varian CP-4900 GC at the Powder Wash site. December 18 calibration run on DCG gas #22933AW	4

LIST OF TABLES

Pa	age
Table 1. Acceptance criteria established by the proposed test protocol for repeatability and reproducibility of sample components	3
Table 2. Acceptance criteria established by the proposed test protocol for repeatability and reproducibility of sample heating values	4
Table 3. Summary of results from the tests of the Fill-and-Empty method conducted at the MRF under optimum conditions	. 14
Table 4. Summary of results from the tests of the Controlled Rate Purge method conducted at the MRF under optimum conditions	. 15
Table 5. Summary of results from the tests of the Helium Pop method conducted at the MRF under optimum conditions	. 15
Table 6. Summary of results from the tests of the Controlled Rate Purge method conducted in November at the Powder Wash field site	. 23
Table 7. Summary of results from the tests of the Helium Pop method conducted in November at the Powder Wash field site.	. 23
Table 8. Summary of results from the tests of the High-Pressure Helium Displacement method conducted in November at the Powder Wash field site	. 24
Table 9. Summary of results from the tests of the Pitot and Bypass method conducted in November at the Powder Wash field site.	. 24
Table 10. Summary of results from the retest of the Fill-and-Empty method conducted in December at the Powder Wash field site.	. 28
Table 11. Summary of results from the retest of the Helium Pop method conducted in December at the Powder Wash field site	. 28
Table 12. Summary of results from the retest of the Pitot and Bypass method conducted in December at the Powder Wash field site.	. 28
Table 13. Comparison of results from all sampling tests performed in this project	. 29
Table D-1. Detailed results from MRF sampling tests, June 18, 2003: Fill-and-Empty method.	. 67

Table D-2.	Detailed results from MRF sampling tests, June 18, 2003: Controlled Rate Purge method.	68
Table D-3.	Detailed results from MRF sampling tests, June 18, 2003: Helium Pop method.	69
Table D-4.	Detailed results from Powder Wash sampling tests, November 10, 2003: Controlled Rate Purge method.	70
Table D-5.	Detailed results from Powder Wash sampling tests, November 10, 2003: Helium Pop method.	71
Table D-6.	Detailed results from Powder Wash sampling tests, November 10, 2003: High-Pressure Helium Displacement method.	72
Table D-7.	Detailed results from Powder Wash sampling tests, November 10, 2003: Pitot and Bypass method.	73
Table D-8.	Detailed results from Powder Wash sampling tests, December 19, 2003: Fill-and-Empty method.	74
Table D-9.	Detailed results from Powder Wash sampling tests, December 19, 2003: Helium Pop method.	75
Table D-10	. Detailed results from Powder Wash sampling tests, December 19, 2003: Pitot and Bypass method.	76

This page is intentionally blank.

1.0 Introduction

The revision of the American Petroleum Institute (API) Manual of Petroleum Measurement Standards (MPMS) Chapter 14.1, *Collecting and Handling of Natural Gas Samples for Custody Transfer* (Reference 1), was completed in 2001. During the revision, the API Chapter 14.1 Working Group compiled a list of unresolved technical issues related to natural gas sampling methodology. An investigation into these technical issues has been ongoing at Southwest Research Institute (SwRI) since 2001, under the Gas Technology Institute (GTI) Measurement Research Program, co-funded by the Gas Technology Institute and the U.S. Minerals Management Service.

This report presents the results of experimental research to evaluate a proposed test protocol to verify the performance of natural gas sampling methods. This protocol is intended to serve as a means of assessing new gas sampling methods for the natural gas industry and should facilitate the development of new and better gas sampling methods. By providing a reliable procedure for new sampling methods to be introduced to the natural gas industry, it will be possible to more accurately determine the energy content of natural gas and reduce the magnitude of errors in natural gas measurements.

A proposed test protocol was drafted by an ad hoc committee of the API Chapter 14.1 Working Group as an addendum to Chapter 14.1. However, until the work described herein was completed, the procedure had not been experimentally validated. The present work involved applying the proposed test protocol to established sampling methods described in GPA (Gas Processors Association) Standard 2261 (Reference 2) and discussed in API Chapter 14.1, as well as to selected new sampling methods. The primary goal of this testing was to evaluate the test protocol. A secondary goal was to assess the ability of several new sampling methods to provide representative gas samples.

Per the requirements of the proposed test protocol, testing of the methods was carried out under both optimum and adverse conditions. For the purposes of this report, "optimum" conditions are considered to be situations where both the pipeline and the ambient temperatures are well above the hydrocarbon dew point (HCDP). On the other hand, "adverse" conditions are defined as situations in which the pipeline temperature is within 5°F of the HCDP, but the ambient temperature is at least 20°F below the HCDP. The testing under optimum conditions was performed at the Southwest Research Institute Metering Research Facility (MRF), and the adverse conditions tests were conducted at the Questar Pipeline Company metering station in Powder Wash, Colorado.

This combination of sampling methods and test conditions was chosen to determine if the protocol could distinguish between acceptable and unacceptable methods, where an acceptable method is considered to be one that produces a representative sample of the flowing gas stream. By using the verification protocol to test currently-recommended sampling methods, it could be determined whether methods known to provide accurate results when performed correctly would pass the tests in the protocol, and whether the acceptance criteria in the protocol were too strict. Including proposed new methods in the test plan allowed for an evaluation of methods that are not already included in the industry standards, but show potential as viable alternatives. The tests also helped to identify any problems with the procedure, and to determine the practicality of the procedure and its ease of implementation in field settings, especially under adverse conditions.

This report describes the testing that was done to evaluate the proposed test protocol and presents the results obtained for both established and new gas sampling methods. The proposed test protocol and the sampling methods that were tested are briefly reviewed in Chapter 2. Chapter 3 presents the results of the sampling tests. This chapter is divided into sections for each test site, and each subsection contains complete documentation of the test facility and conditions, as well as a summary of the results obtained. Chapter 4 concludes the report with a comparison of the results from all of the sampling tests and an assessment of the proposed test protocol itself. For reference purposes, several items have been included in the appendices of this report. These items include the complete text of the proposed test protocol

(Appendix A), procedures for the new sampling methods (Appendix B), gas chromatograph setup and calibration data (Appendix C), and a detailed tabulation of the results from all of the sampling tests (Appendix D).

2.0 Test Protocol and Sampling Methods

This chapter contains a brief overview of the proposed test protocol and presents the sampling methods that were considered for use in this investigation. The complete test protocol and detailed procedures for the new sampling methods may be found in Appendices A and B, respectively.

2.1 Performance Verification Test Protocol

A draft of the proposed test protocol used for the present testing may be found in Appendix A. As of the date of this report, the proposed test protocol was in the API ballot process. It is expected that the results and experience obtained from this testing will be used to revise the protocol before final publication.

The proposed test protocol requires that the gas samples be evaluated in terms of both repeatability and reproducibility. For purposes of this protocol, the API definition of repeatability is used: the comparison of back-to-back analyses using the same sample, chromatograph and operator (Reference 1). Reproducibility is defined as the comparison between the analysis of the flowing gas stream itself and the analysis of a spot or composite sample taken from the same stream. For each sampling method under evaluation, the protocol requires that a minimum of five samples be taken, and that each sample be analyzed at least three times. Repeatability and reproducibility of all gas stream components (typically C₁ through C₉, CO₂, and N₂) and the heating value are evaluated. (The methods used to analyze the data for these tests will be discussed in more detail in Section 3.1.3.) Results of successive analyses of each sample are compared to judge the repeatability of the sample; reproducibility is assessed by determining how well a sample analysis matches the analysis of the flowing gas stream, determined with an online or portable gas chromatograph, and analyzed at the same time that the sample is drawn from the flowing gas stream. The acceptance criteria for repeatability and reproducibility established by the proposed test protocol for composition and heating value are shown in Table 1 and Table 2. The values for the individual components are taken directly from API Chapter 14.1, Appendix E.

Table 1. Acceptance criteria established by the proposed test protocol for repeatability and reproducibility of sample components.

Repeata	bility Criteria	Reproducibility Criteria		
Mol % Max. Allowed Concentration Deviation (± Mol %)		Mol % Concentration	Max. Allowed Deviation (± Mol %)	
0 to 1	0.02	0 to 1	0.04	
> 1 to 5	0.10	> 1 to 5	0.13	
> 5 to 15	0.18	> 5 to 15	0.26	
> 15 to 30	0.28	> 15 to 30	0.38	
> 30 to 50	0.40	> 30 to 50	0.50	
> 50	0.52	> 50	0.63	

Table 2. Acceptance criteria established by the proposed test protocol for repeatability and reproducibility of sample heating values.

Repeatability Criteria	Reproducibility Criteria
1 Btu/scf	3 Btu/scf

Some key features and requirements of the test protocol are as follows:

- The protocol provides acceptance criteria for repeatability (of multiple samples from the same sample cylinder) and reproducibility (of the flowing stream composition by the spot samples).
- The same gas chromatograph is used to analyze the flowing gas stream itself and the spot or composite samples taken from the stream, to eliminate any bias error caused by using different chromatographs. The chromatograph, sample delivery system, and calibration procedures must comply with the requirements of API Chapter 14.1, Appendix E.
- Cleanliness of all analysis equipment must be verified before tests.
- A proposed sampling method is to be tested on at least two different gas compositions, under both optimum and adverse conditions.
- The hydrocarbon dew point of the gas stream must be measured before the tests, and equipment must be kept well above the dew point to prevent sample distortion.
- Verification that the chosen sampling location has a steady flow rate and a stable gas composition is required prior to the sampling tests.
- Specific reporting requirements are given to ensure proper documentation of the procedure and results.

2.2 Sampling Methods

The API Chapter 14.1 Working Group identified a total of nine sampling methods as candidates for testing using the protocol. Of these, five were established methods that are currently recommended in API Chapter 14.1, and the remaining four were proposed new methods. As the project progressed, it was decided not to test some of the methods, and results were ultimately obtained for three established methods and three new methods. The sampling methods that were used and those that were considered but not tested are discussed in the following sections.

2.2.1 Established Sampling Methods Tested Using the Protocol

The proposed test protocol was used to test three of the methods described in GPA 2261 (Reference 2) and listed in API Chapter 14.1 as acceptable for use. The established sampling methods that were tested as a part of the current project are as follows:

- Purging Fill-and-Empty Method
- Helium Pop Method
- Purging Controlled Rate Method

For these methods, the procedures given in the 2003 draft of GPA Standard 2166 were followed. As its name suggests, the Fill-and-Empty method involves alternately filling and emptying the sample cylinder a specified number of times before filling it with the final gas sample. This purging cycle serves to remove any helium blanket gas or other residual contents from the sample cylinder before the final sample is taken. For the Helium Pop method, the sample cylinder is evacuated and charged above atmospheric pressure using a small amount of helium, to prevent air leaks into the cylinder, before the cylinder is filled with the gas sample. The Controlled Rate Purge method is similar to the Fill-and-Empty procedure, except that natural gas flows continuously through the sample cylinder to purge it for a specified period of time before a gas sample is collected.

The Fill-and-Empty and Helium Pop methods were chosen for testing since they are commonly used, and since experience within the API 14.1 Working Group indicated that these methods would perform well under relatively adverse conditions. Although the Controlled Rate Purge method is listed in API Chapter 14.1 as acceptable for use, this method was expected to do poorly when used under adverse conditions, and it was included to test the ability of the verification protocol to distinguish between acceptable and unacceptable methods. Informal experience within the Working Group suggested that under adverse conditions, heavy hydrocarbons would condense in the sample cylinder as gas was purged through the cylinder, leading to samples with higher heating values than the actual flowing stream.

2.2.2 Proposed New Sampling Methods Tested Using the Protocol

The verification test procedure was also applied to three new sampling methods proposed to the API Chapter 14.1 Working Group:

- Pitot and Bypass Method proposed by Fred Van Orsdol, SPL Corporation
- High-Pressure Helium Displacement Method proposed by Eric Fritz, Natural Gas Pipeline Company of America
- Modified Helium Pack Method proposed by R. Mark Haefele, BP

Detailed procedures for these three methods may be found in Appendix B. The Pitot and Bypass method is a modification of the Controlled Rate Purge method designed to eliminate venting of the purge gas to the atmosphere. In this method, the outlet of the sample cylinder is connected to a second tap on the pipeline, so that during purging, flow passes through the sample cylinder and reenters the pipeline downstream of the gas sampling point. The High-Pressure Helium Displacement method also follows a procedure similar to the Controlled Rate Purge method, except that the sample cylinder is initially charged with helium to a pressure greater than the pipeline pressure. When the valves are initially opened, the helium purges the sample probe and flows into the pipeline. The Modified Helium Pack method is also a procedure similar to the Helium Pop method, except that the sample cylinder is evacuated after attachment to the pipeline, thus eliminating the emission of gas to the atmosphere. All of these methods use a sample cylinder that is initially pressurized with helium to a pressure above the pipeline pressure so that the sample probe can be back flushed prior to sampling.

2.2.3 Sampling Methods Considered but Not Tested

Three out of the nine sampling methods that were initially proposed for testing under the verification protocol were not tested due to limitations of the project budget and schedule. The methods that were not tested are as follows:

- Water Displacement Method GPA 2166 (Reference 2)
- Glycol Displacement Method GPA 2166 (Reference 2)
- Two-Stage Absorption Method proposed by Chris Cowper, EffecTech Ltd.

The two GPA methods were eliminated because they are less commonly used than the other GPA methods tested. The Two-Stage Absorption method was not tested due to its complexity, and due to the fact that the API 14.1 Working Group concluded that its purpose was not in line with the goals of this project.

3.0 Sampling Tests

The sampling tests performed to evaluate the proposed test protocol were performed at two sites. The testing under optimum conditions was performed at the SwRI Metering Research Facility, while the adverse condition tests were conducted at a Questar Pipeline metering station in Powder Wash, Colorado. One feature of the proposed test protocol is that it requires extensive documentation of the tests and results. In accordance with those requirements, this chapter contains detailed information on the facilities and conditions found at each test site, along with the results obtained from the testing. This chapter concludes with an overall comparison of the results from all of the sampling tests, and an assessment of the proposed test protocol itself.

3.1 Verification Tests Performed Under Optimum Conditions

The testing under optimum conditions was conducted at the SwRI Metering Research Facility. During this testing both the pipeline and ambient temperature were well above the HCDP. At the MRF, the Fill-and-Empty method, the Helium Pop method, and the Controlled Rate Purge method were tested. The original project plans called for the three new sampling methods to also be tested at the MRF, but equipment problems discussed below required a revision to the scope of work, and it was decided to test the new methods only at the field site. Since the conditions at the field site were far less favorable than those at the MRF, testing the new methods only at the field site still provided a worst-case evaluation of the new methods.

3.1.1 Facility and Equipment

The testing was performed in lean gas (nominally 1,050 Btu/scf) using the High Pressure Loop (HPL) at the MRF. The HPL was configured for the sampling tests by installing several existing pipe spools equipped with fittings for the sample probes in the test section of the loop. Figure 1 is a schematic of the test facility layout showing where the various pieces of equipment were installed in the HPL test section. All of the sampling locations were located at least 8 pipe diameters downstream of any component that could create a flow disturbance. A photograph of the facility taken during the tests is shown in Figure 2.

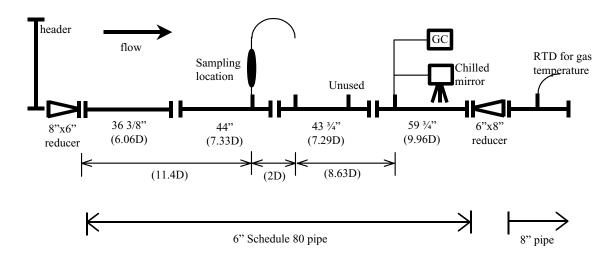


Figure 1. Schematic of the MRF test section showing the piping arrangement and spot sampling locations.



Figure 2. MRF test section piping configured for the sampling tests. The schematic for this setup is shown in Figure 1.

Figure 3 is a photograph of the sampling apparatus used for tests of the Controlled Rate Purge method. The arrangement of the equipment for the other methods was similar to the arrangement shown in this figure. The sample probes had angle-cut ends and were sized so that the tip of the probe was located in the center one-third of the pipe. Whitey® ball valves were installed on the sample probes and at the end of the pigtail. In keeping with the common practice, the API 14.1 Working Group requested that the sample cylinders used for the testing be equipped with YZ® needle valves at each end. All connections and pigtails were made with ¼" OD stainless steel tubing and ¼" NPT fittings. For the Controlled Rate Purge method, a drilled plug with a 0.02-inch diameter bore was installed at the end of the pigtail, in accordance with API Chapter 14.1. A separator [as described in GPA 2166 (Reference 2)] was not included in any of the sampling systems for this testing, since the flowing gas temperature and equipment temperatures were all well above the HCDP of the gas.

Preparation of the sampling equipment followed the procedures given in the proposed test protocol. All of the sample cylinders, valves, probes, and tubing were steam cleaned prior to use. After cleaning, all of the sample cylinders were evacuated, and cylinders to be used for the Helium Pop method were charged with helium. A total of fifteen 300-cc sample cylinders were prepared for testing, so that three different methods could be tested before cylinders had to be reused. To verify the cleanliness of the sample cylinders, two of the cylinders were charged with helium (99.999% purity) to 50 psig and heated to 180°F for 12 hours. Gas Chromatographic (GC) analysis of the contents of these cylinders showed no peaks in the chromatograms, hence, it was concluded that the cleaning process had left no residual hydrocarbons in the cylinders.

To gather information about the test conditions and sampling equipment, the standard instrumentation at the HPL was used, along with some additional thermocouples installed at several key locations in the gas sampling system. Exposed-junction, type T thermocouples were taped to the sample probe just above the pipeline, the tubing just below the sample cylinder inlet, the GC sample probe just above the pipeline, and the GC inlet. Surface temperature data from these sensors was read and logged by an HP Model 34970A data logger at one-second intervals. In addition to these measurements, the HPL instrumentation recorded the temperature, pressure and flow rate of the gas stream, and the ambient

temperature. The temperature and pressure of the gas stream were measured using Rosemount Model 3144 and 3051C transmitters, respectively. The flow rate was determined using the HPL critical flow nozzles, and verified using two reference turbine meters.

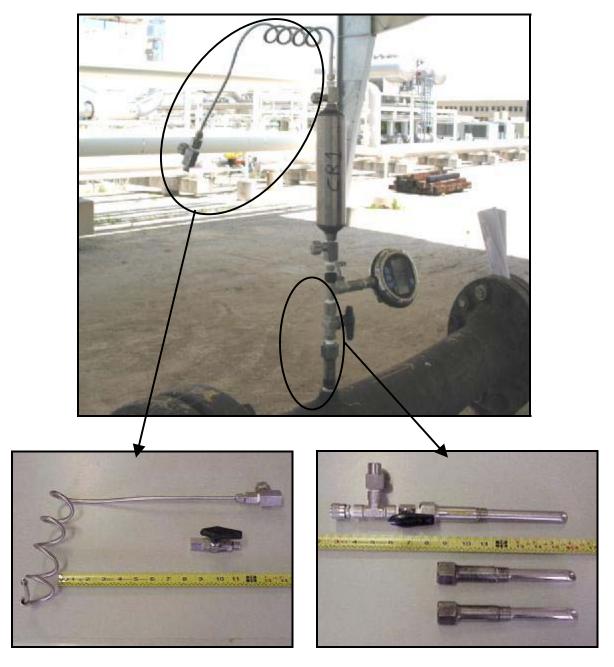


Figure 3. Sampling equipment used in tests of the Controlled Rate Purge method at the MRF. Bottom left, pigtail and end valve; bottom right, sample probes with isolation valve and pressure gauge connection. The scale on the tape measure is in inches.

As required by the proposed test protocol, the HCDP of the gas stream was determined by using a manual chilled mirror tester (dew scope) equipped with a video camera. Figure 4 shows the dew scope (Chandler Engineering Chanscope II, Model 13-1200-C-N-1) in use during the tests at the MRF. The

temperature sensor in the dew point tester was calibrated, traceable to NIST, before using the device. Measurements of the dew point were made independently by two technicians to confirm the readings.

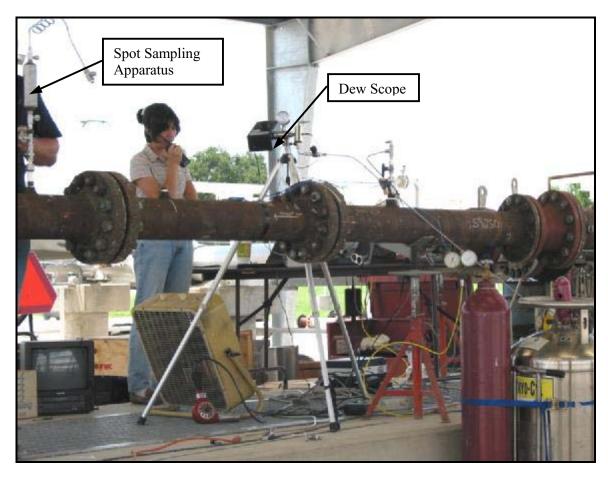


Figure 4. Dew scope connected to the MRF test section for determination of the gas stream HCDP.

It was originally planned for all of the gas composition analyses to be performed with a portable gas chromatograph that was loaned by Questar for use in this project. This GC was to be used for analyses of both the flowing gas stream and the gas samples, to eliminate any potential biases that could be caused by using different instruments for the two analyses. Prior to the start of the first sampling tests, the GC was taken to the MRF calibration laboratory and all of the preparation, calibration, and verification procedures of the proposed sampling verification protocol were performed. Although the GC met all of the requirements of the protocol, problems were encountered when the GC was moved outdoors to the HPL for the sampling tests. During these tests, the calibration drifted and the instrument failed to produce repeatable analyses of the flowing gas stream. The cause of the drift was traced to changing ambient conditions. Figure 5 contains two chromatograms, one taken in the morning, and the other taken in the afternoon, illustrating the drift that was observed.

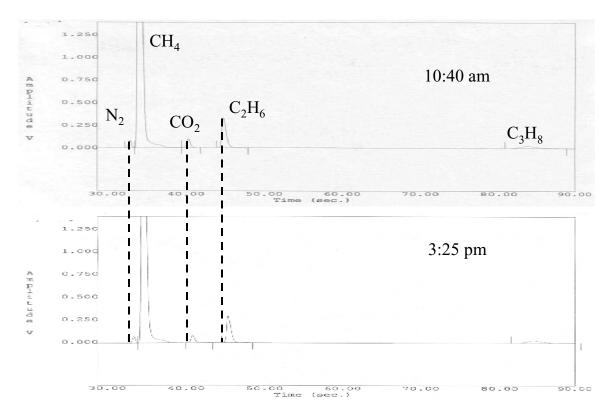


Figure 5. Stream analyses from 10:40 am and 3:25 pm on June 18, illustrating the drift that was observed in the portable GC during the MRF tests.

Instead of using the portable GC, it was decided to use the MRF on-line GC, which was also operating during the sampling tests. The MRF GC is a Daniel Model 2350 capable of analyses to C₉+, with analysis software and a sample delivery system that also complies with all of the requirements of API Chapter 14.1. The sample probe for the Daniel GC is located far downstream of the test section, and upstream of the critical flow Venturis used as the reference flow meters for the test facility. The MRF GC is located outdoors, but the columns are contained in insulated ovens for year-round stable performance. Heating of the sample cylinders or other sampling equipment was not required for these tests, as ambient temperatures were far above the HCDP. Further details of the analysis setup may be found in Appendix C of this report, which contains the API Chapter 14.1 inspection checklist for the sample analysis system.

The work to verify that the portable GC met all of the requirements of the sampling protocol was repeated for the MRF GC. The procedures given in the sampling protocol were again followed for calibration of the MRF GC. Since it is used for routine testing at the MRF, the Daniel GC is calibrated daily on a 1,030 Btu/scf gas that was prepared in accordance with the requirements of the current revision of API Chapter 14.1, Section 16. Analyses were repeatable to within 0.02 mol% for methane and to within smaller limits for the other components. The MRF chromatograph was also tested on a separate certified gas blend to determine its ability to reproduce known gas compositions. Analyses of the "unknown" gas reproduced its certified composition to within 0.05 mol% for methane and less for the other components. All repeatability and reproducibility values were within API Chapter 14.1 Appendix E limits. Detailed information on the GC calibration, including fidelity plots, is included in Appendix C.

3.1.2 Test Conditions

Tests of the Fill-and-Empty method, the Helium Pop method, and the Controlled Rate Purge

method were conducted on June 18, 2003. The specific procedures used for the testing of these methods at the MRF can be found in the 2003 draft revision of GPA 2166, which is expected to be published in 2004. The actual procedures have changed little from the 1986 edition of GPA 2166. For tests of the Fill-and-Empty method, three fill-and-empty cycles were completed before the final sample was collected. For the Controlled Rate Purge method, the sample cylinder was purged for 70 seconds prior to collection of the sample.

The gas used for the testing was obtained from the MRF storage vessels and recirculated in the flow loop to ensure a constant gas composition during the tests. Since no gas was added or removed from the loop while the sampling tests were being performed and all temperatures were significantly above the HCDP, it can be assumed that the gas composition in the system was stable during the testing.

As required by the proposed test protocol, the HCDP of the gas stream was measured immediately prior to collecting the gas samples and again at the conclusion of the testing. During attempts to measure the hydrocarbon dew point, water vapor condensed on the chilled mirror first, making determination of the HCDP difficult. In one run, water condensation was observed at 37°F, and no clear evidence of hydrocarbon liquids was found until the temperature was well below 0°F. For the test conditions, the HCDP was predicted using equations of state to be 27°F. Consequently, a dew point of 37°F was taken as a conservative estimate of the HCDP for the tests.

The flow rate and system pressure were monitored during testing to verify that they remained stable. Values of the line pressure and gas velocity during the periods that the three sampling methods were tested are shown in Figure 6. A steady flow rate of approximately 435 acfm in the loop was maintained during testing through the use of critical flow Venturis that served as the reference flow meters for the test facility. The gas stream pressure varied only slightly, between 1,009 and 1,014 psia.

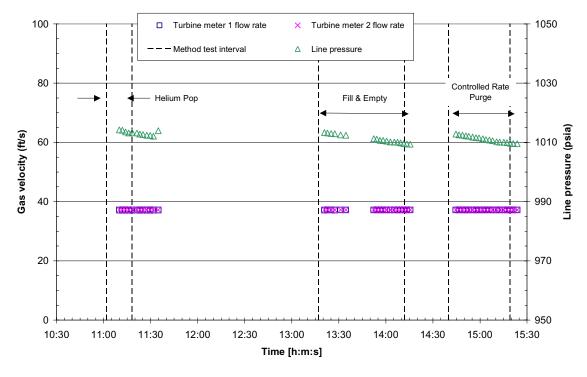


Figure 6. Gas velocity and pressure in the loop during the sampling tests conducted at the MRF. Vertical dashed lines show intervals during which samples were drawn using the various methods. Flow was in a 6" diameter Schedule 80 pipe.

The local temperatures of the sampling hardware, along with the gas stream and ambient temperature, are plotted in Figure 7 for the periods that the samples were drawn using the three test methods. These data show that none of the sampling equipment dropped below 71°F during the tests. Since the gas stream temperature and the equipment temperatures were all significantly above the HCDP (conservatively estimated to be 37°F, as discussed above), heating of the sample lines was not necessary.

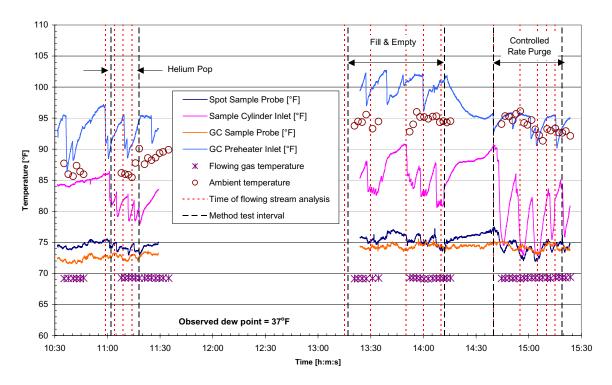


Figure 7. Equipment and gas temperatures during the sampling tests conducted at the MRF. Black vertical lines with long dashes indicate intervals during which samples were drawn using the various methods. Red vertical lines with shorter dashed lines indicate times when GC analyses of the flowing stream were obtained.

3.1.3 Results

For each sampling method tested, five gas samples were collected and analyzed. Each sample was collected in a separate 300 cc sample cylinder using the procedure appropriate for the method. After all of the samples had been collected, the gas samples were analyzed using the MRF GC. As required by the protocol, results of the analysis of each cylinder were compared to an analysis of the flowing stream, also made with the MRF GC nearest to the time that the sample was drawn. Because ambient conditions were 40°F or more above the conservative dew point of the HPL gas, and sections of the GC sample delivery lines were heat traced to 120°F, it was not deemed necessary to heat the gas samples prior to the analysis. The contents of each sample cylinder were analyzed six times. To be sure that the GC and sample delivery system had been purged of the gas sample from the previous run, only the results of the last three analyses of each cylinder were used to evaluate the method.

To illustrate the method used to evaluate the results of each sampling method, consider three successive GC analyses of a gas sample obtained using a particular sampling method. Let the analysis results obtained in order from a single sample cylinder be A_1 , A_2 , and A_3 , where A_1 , A_2 , and A_3 represent

either the concentration of a single component in the analysis, or the heating value of the gas composition in the analysis. The repeatability deviation for a particular component (or the heating value) is computed as the maximum absolute difference between successive pairs of values. In terms of the notation just introduced.

Repeatability Deviation =
$$max\{|A_1 - A_2|, |A_2 - A_3|\}$$
. (Eq. 1)

The reproducibility deviation for a particular component (or the heating value) is based on the maximum absolute difference obtained when comparing each of the three analyses to the value obtained from the GC analysis of the gas stream taken at approximately the same time as the sample. If A_{STRM} is the concentration of one component, or the heating value of the gas stream, then

Reproducibility Deviation =
$$max\{|A_1 - A_{STRM}|, |A_2 - A_{STRM}|, |A_3 - A_{STRM}|\}$$
. (Eq. 2)

The results obtained from the three sampling methods tested at the MRF are summarized in Table 3 through Table 5. The complete results of the analyses of each sample have been included in Appendix D. In these tables, the first column identifies the sample cylinder used in testing the method. The second column identifies any component that failed to meet the repeatability criteria. If all components are within the specified limits, then the results are reported as "All OK". The actual deviations for each component may be found in the data included in Appendix D. The next column shows the maximum repeatability deviation in heating value, computed from Equation 1. The last two columns of the tables report the reproducibility results in a format similar to the repeatability results. Note, as discussed above, that the deviations reported in these tables and in Appendix D are unsigned (i.e., only the absolute value of the differences have been considered).

All of the samples taken using the three methods met the repeatability and reproducibility requirements for the components and the heating value. Thus, it may be concluded that, under optimum conditions, the three methods produced representative samples of the gas stream to within the required limits of the proposed test protocol. These results will be discussed in more detail in Section 3.3, where they will be compared to the results obtained from the other sampling tests.

Table 3. Summary of results from the tests of the Fill-and-Empty method conducted at the MRF under optimum conditions.

	Repeatability		Repro	ducibility
	Components not Meeting Criteria	Max. Heating Value Deviation (Btu/scf)	Components Not Meeting Criteria	Max. Heating Value Deviation (Btu/scf)
Sample Cylinder FE1	All OK	0.14	All OK	0.95
Sample Cylinder FE2	All OK	0.15	All OK	0.86
Sample Cylinder FE3	All OK	0.05	All OK	0.26
Sample Cylinder FE4	All OK	0.19	All OK	0.22
Sample Cylinder FE5	All OK	0.10	All OK	0.61

Table 4. Summary of results from the tests of the Controlled Rate Purge method conducted at the MRF under optimum conditions.

	Repeatability		Reproducibility	
	Components not Meeting Criteria	Max. Heating Value Deviation (Btu/scf)	Components Not Meeting Criteria	Max. Heating Value Deviation (Btu/scf)
Sample Cylinder CR1	All OK	0.24	All OK	0.77
Sample Cylinder CR2	All OK	0.29	All OK	1.43
Sample Cylinder CR3	All OK	0.05	All OK	0.97
Sample Cylinder CR4	All OK	0.63	All OK	0.69
Sample Cylinder CR5	All OK	0.70	All OK	0.73

Table 5. Summary of results from the tests of the Helium Pop method conducted at the MRF under optimum conditions.

	Repeatability		Reproducibility	
	Components not Meeting Criteria	Max. Heating Value Deviation (Btu/scf)	Components Not Meeting Criteria	Max. Heating Value Deviation (Btu/scf)
Sample Cylinder HP1	All OK	0.07	All OK	0.96
Sample Cylinder HP2	All OK	0.04	All OK	0.99
Sample Cylinder HP3	All OK	0.60	All OK	0.87
Sample Cylinder HP4	All OK	0.03	All OK	0.80
Sample Cylinder HP5	All OK	0.21	All OK	0.84

3.2 Verification Tests Performed Under Adverse Conditions

For tests of the sampling methods under adverse conditions, a field site was desired with a rich gas stream (1,200-1,400 Btu/scf) at line conditions just above the HCDP. The field site was also required to have a stable gas composition and adequate infrastructure for performing the testing (sampling ports, pipeline instrumentation, an accessible GC, etc.). The site selection committee sent questionnaires to a number of companies, and received information on seventeen candidate sites for the field tests.

The site chosen for the field testing of the proposed test protocol is a Questar Pipeline metering station in Powder Wash, Colorado. The testing was performed under adverse conditions during which the pipeline temperature was at or just above the HCDP and the ambient temperatures were well below the HCDP. At the Powder Wash site, the following methods were tested: Fill-and-Empty, Helium Pop, Controlled Rate Purge, Pitot and Bypass, and High-Pressure Helium Displacement. An attempt was made to test the Modified Helium Pack method, but due to the cold conditions, the vacuum pump needed for this method would not function, and a second vacuum pump also failed, so that testing of this method was not possible.

3.2.1 Facility and Equipment

The testing was performed in rich gas (nominally 1,200 Btu/scf) at the Questar metering station in Powder Wash, Colorado. This is the same site used during the composite sampler tests conducted in 1999 and 2000 and discussed in Reference 3. The samples were collected from a straight section of 8-inch-diameter pipe located immediately upstream of an orifice meter. This section of pipe had four sampling locations located five pipe diameters apart. A photograph of the facility taken during the tests is shown in Figure 8. In the direction of flow, the first pair of sampling locations contained the curved probes used for the Pitot and Bypass method. The next sampling location was equipped with a straight probe that was used for the other sampling methods tested. The fourth sampling location at the downstream end of the pipe was used for the dew point tester and the gas chromatograph. The spacing between the sampling locations was sufficient to place each probe at least eight characteristic diameters downstream of any object creating a flow disturbance, where the characteristic diameter is based on the scale of the object creating the disturbance (e.g., the diameter of an upstream probe).

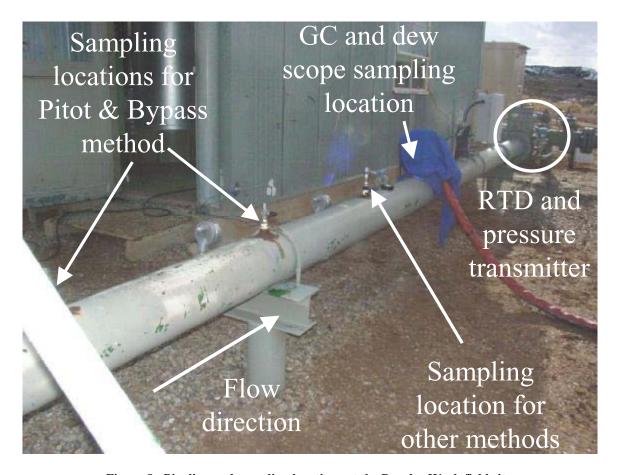


Figure 8. Pipeline and sampling locations at the Powder Wash field site.

The sampling arrangements used for most of the methods are shown in Figure 9 and Figure 10. The sampling hardware (valves, tubing, sample cylinders, etc.) from the MRF tests was also used for performing the same tests at the Powder Wash site. Questar provided some additional 300-cc sample

cylinders, valves and probes for tests of the new sampling methods. As much as practical, the configuration of the sampling equipment from the MRF tests was duplicated for the Powder Wash tests. Ball valves were installed on the sample probes and needle valves were used on the sample cylinders and at the end of the pigtail. The only exception to this was for the Pitot and Bypass method, which required ball valves on the sample cylinders and at both probes. All connections and pigtails were made with ¼" OD stainless steel tubing and ¼" NPT fittings. For the Controlled Rate Purge method and the High-Pressure Helium Displacement method, a drilled plug with a 0.02-inch diameter bore was installed at the end of the pigtail. A separator [as described in GPA 2166 (Reference 2)] was not included in any of the sampling systems, at the request of the API 14.1 Working Group.

Figure 11 shows the sampling probes that were used. The Pitot and Bypass method required a pair of curved probes. These probes were manufactured by Welker Engineering and were designed so that the curved end could be inserted through the existing fittings on the pipe. For all of the other methods, straight sample probes with angle-cut ends were used. All of the sample probes were sized so that the tip of the probe was located in the center one-third of the pipe.







Figure 9. Configuration of the equipment used for collecting samples at the Powder Wash field site. Left, Controlled Rate Purge; center, Fill-and-Empty; right, High-Pressure Helium Displacement.



Figure 10. Configuration of the equipment used for collecting samples with the Pitot and Bypass method at the Powder Wash field site.





Figure 11. Sampling probes used for the Powder Wash tests. Left, curved probes for the Pitot and Bypass method; right, example of a straight probe used for the other sampling methods.

Preparation of the sampling equipment again followed the procedures given in the proposed test protocol. Enough 300 cc sample cylinders were prepared so that all six of the methods could be tested at the field site. All of the sample cylinders, valves, probes, and tubing from the MRF test were steam cleaned prior to reuse at the field site. The equipment provided by Questar was cleaned with acetone. Prior to the start of tests, a subset of cleaned sample cylinders were charged with helium (99.999% purity), and then analyzed to verify that the portable GC, sample cylinders, and sample delivery tubing were clean and free of contaminants. After cleaning, all of the sample cylinders were evacuated, and the cylinders to be used for the Helium Pop method and the three new sampling methods were pre-charged with helium as specified in their respective sampling procedures.

The HP Model 34970A data logger was again used to monitor and record (at one-second intervals) temperatures obtained with surface-mount type T thermocouples attached to the sample probe, the sample cylinder inlet, the gas chromatograph (GC) sample probe, and the GC inlet. An additional, standard Type T thermocouple was used to measure the ambient temperature. The temperature, pressure, and flow rate of the gas stream were obtained from transmitters and a flow computer permanently located at the site.

The HCDP of the gas stream was measured using a chilled mirror device provided by Questar. As required by the proposed test protocol, the dew scope had a NIST traceable temperature sensor calibration. Measurements of the dew point were made independently by two technicians to confirm the readings.

All of the gas analyses at the Powder Wash site were performed using a Varian Model CR-4900 portable gas chromatograph. This GC is capable of analyses to C₉₊ and it was verified that the chromatograph and sample delivery system complied with all of the requirements of API Chapter 14.1. The GC was connected to a sample probe located downstream of the spot sample location as shown in Figure 8. The GC was located in a heated vehicle, and the line connecting the GC to the pipeline was heat traced along its entire length. Further details of the analysis setup may be found in Appendix C of this report, which contains the API Chapter 14.1 inspection checklist for the sample analysis system.

Validation of the portable GC was carried out using the procedures given in the proposed sampling protocol. The GC was calibrated on a 1,200 Btu/scf gas that was prepared in accordance with the requirements of the current revision of API Chapter 14.1, Section 16. The chromatograph was also tested on a separate certified gas blend to determine its Warren reproducibility. All repeatability and reproducibility values were within API Chapter 14.1 Appendix E limits. As will be discussed in more detail below, some additional sampling tests were performed following the first round of tests completed in November. The portable GC was calibrated prior to these additional tests, and all values were again within the Appendix E limits, except for CO₂, which was 0.01 mol% high. Detailed information on the GC calibrations, including fidelity plots, is included in Appendix C. The calibration gases were analyzed using a separate GC to confirm their composition before they were used to calibrate the Varian GC used for the protocol analyses.

3.2.2 Test Conditions

Tests of the Fill-and-Empty, Helium Pop, Controlled Rate Purge, Pitot and Bypass, and High-Pressure Helium Displacement methods were conducted on November 10, 2003. The specific procedures used for these methods at the Powder Wash site can be found in the 2003 draft revision of GPA 2166 and in Appendix B. For the Fill-and-Empty method, three fill-and-empty cycles were completed before the final gas sample was collected. For tests of the Controlled Rate Purge method, the sample cylinder was purged for 70 seconds prior to collection of the sample. As noted in the table of results below, some Pitot and Bypass samples were taken after a 60 second purge time, while others were taken after a 90 second purge time.

The gas stream was monitored before and during the testing to determine the stability of the gas

composition and the flowing conditions in the pipeline. Figure 12 shows measurements of the stream heating value and nitrogen content at one-hour intervals taken over the course of several days around the time of the tests. The nitrogen content remained fairly constant, but the heating value exhibited a regular fluctuation of approximately ±10 Btu/scf over the course of several days, suggesting that the line temperature may have been influencing the gas composition. This was also observed during the composite sampler tests conducted in 1999 and 2000 and discussed in Reference 3. The Powder Wash metering station is located just downstream of a separation facility, so that the gas stream temperature is typically very close to the HCDP. The tandem changes in stream temperature changes and heating value reflect the fact that the gas leaving the separator is normally at or just above the HCDP temperature. However, the period of the fluctuations is very long compared with the time interval over which all samples were taken using a given test method, thus, the composition was essentially stable while tests of each sampling method were being performed.

The HCDP of the gas stream was measured immediately prior to collecting the gas samples and determined to be 69°F, approximately the same as the flowing stream temperature. An attempt was made to measure the HCDP after tests, but the tests were concluded after sunset, and the dew scope used at the site relied on ambient lighting to illuminate the chilled mirror, so a post-test measurement was not possible.

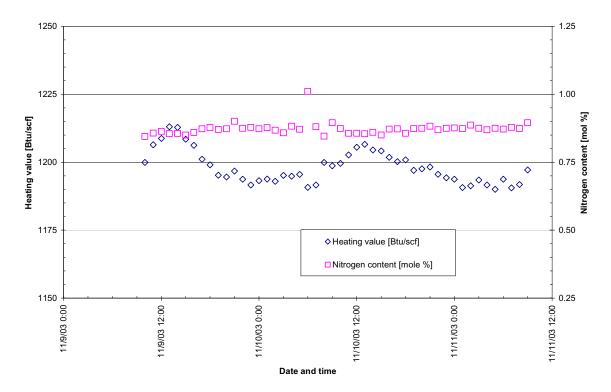


Figure 12. Long-term trends in flowing stream heating value and nitrogen content around the time of the sampling tests conducted in November at the Powder Wash field site.

Detailed records of the line pressure and flowing gas velocity during the times that the sampling methods were tested are shown in Figure 13. For this period, the line pressure remained fairly constant at approximately 580 psia, and the average flow rate was 7,670 Mscfd with a variation (maximum to minimum) of $\pm 3.3\%$ about this mean.

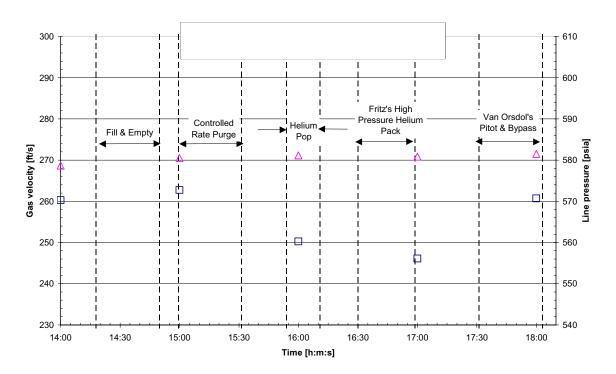


Figure 13. Gas velocity and pressure in the pipeline during the sampling tests conducted in November at the Powder Wash field site. Vertical dashed lines show intervals during which samples were taken using the various sampling methods. Flow was in an 8" diameter pipe.

Because the ambient temperature at the site was well below the HCDP of the gas stream, all of the sampling equipment was kept in heated storage containers until it was used to obtain a sample. Although the sample cylinders were insulated to keep them warm outside of the storage containers, insulation was not available during the November tests for the valves and lines connected to the cylinder, as shown in Figure 14.

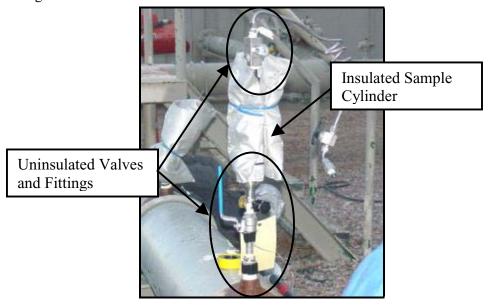


Figure 14. Typical sampling arrangement at the Powder Wash field site showing which portions of the system were not insulated during the November tests. The attached lines and valves were insulated during the December retests.

The local temperatures of the sampling hardware, along with the gas stream and ambient temperature, are plotted in Figure 15 for the periods that the samples were taken using the various methods. These data show that all of the monitored locations on the sampling equipment were below the HCDP during the tests, as might be expected, since these regions were not insulated. The use of sampling equipment with temperatures below the HCDP and the fact that the gas was likely near saturation (as this site was downstream of a separator) may have contributed to the poor performance of some of the methods tested.

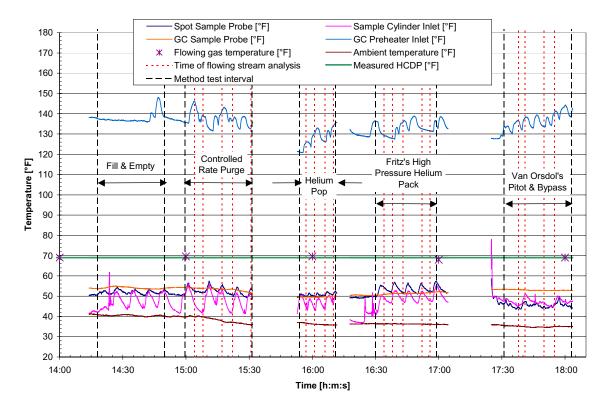


Figure 15. Equipment and gas temperatures during the sampling tests conducted in November 2003 at the Powder Wash field site. Black vertical lines with long dashes indicate intervals during which samples were drawn using the various methods. Red vertical lines with shorter dashed lines indicate times when GC analyses of the flowing stream were obtained.

3.2.3 Results

For each sampling method that was tested, five gas samples were collected and analyzed. Each sample was collected in a separate 300-cc sample cylinder using the procedure appropriate for the method. After all of the samples had been collected, the gas samples were heated to 125°F overnight at the Questar lab, and analyzed three times using the same GC that was used to analyze the flowing gas stream. Before analysis of the contents of each cylinder, helium was used to purge the GC and sample delivery system of the gas from the previous run.

During the process of analyzing the samples, an air leak was discovered in the sample delivery system. This leak was not found during the preparations specified in the proposed test protocol. As a result, all of the cylinders that had been analyzed prior to the discovery of the leak were reanalyzed after the leak was repaired. In the case of the samples obtained with the Fill-and-Empty method, there was not enough gas remaining in any of the sample cylinders to perform another analysis. For most of the other

methods, contents of only one sample cylinder were lost.

The results obtained from the sampling methods tested under adverse conditions are summarized in Table 6 through Table 9. The complete results of the analyses of each sample have been included in Appendix D. The format of these tables is identical to the tables presented and discussed in Section 3.1.3. To assist in interpreting the reproducibility results, components not meeting the criteria of the proposed test protocol have been identified as being either "high" or "low" to indicate how the values compared to the reference values of the gas stream. Values in bold red type are outside the acceptance criteria of Table 1 and Table 2. The Controlled Rate Purge and High-Pressure Helium Displacement methods failed the reproducibility tests, and some samples taken using the Helium Pop and the Pitot and Bypass methods passed, while others did not. These results will be discussed in more detail in Section 3.3, where they will be compared to the results obtained from the other sampling tests.

Table 6. Summary of results from the tests of the Controlled Rate Purge method conducted in November at the Powder Wash field site.

	Repeatability		Reproducibility	
	Components not Meeting Criteria	Max. Heating Value Deviation (Btu/scf)	Components Not Meeting Criteria	Max. Heating Value Deviation (Btu/scf)
Sample Cylinder CR1	N_2	0.86	high- N_2 , C_6	8.78
Sample Cylinder CR2	No data available		No data available	
Sample Cylinder CR3	N_2	0.25	high- N ₂ low- CO ₂	5.04
Sample Cylinder CR4	All OK	0.12	high- C ₃	7.07
Sample Cylinder CR5	All OK	0.50	high- C ₃ , iC ₄	6.61

Table 7. Summary of results from the tests of the Helium Pop method conducted in November at the Powder Wash field site.

	Repeatability		Reproducibility	
	Components not Meeting Criteria	Max. Heating Value Deviation (Btu/scf)	Components Not Meeting Criteria	Max. Heating Value Deviation (Btu/scf)
Sample Cylinder HP1	All OK	0.16	high- N ₂	2.50
Sample Cylinder HP2	All OK	0.20	high- N ₂	3.17
Sample Cylinder HP3	All OK	0.03	All OK	3.82
Sample Cylinder HP4	No data available		No data available	
Sample Cylinder HP5	All OK	0.45	high- N ₂	2.79

Table 8. Summary of results from the tests of the High-Pressure Helium Displacement method conducted in November at the Powder Wash field site.

	Repeatability		Reproducibility	
	Components not Meeting Criteria	Max. Heating Value Deviation (Btu/scf)	Components Not Meeting Criteria	Max. Heating Value Deviation (Btu/scf)
Sample Cylinder EF1	All OK	0.51	high- C ₅ to C ₇	8.50
Sample Cylinder EF2	All OK	0.54	<i>high</i> - iC ₅ , C ₆ , C ₇	9.32
Sample Cylinder EF3	All OK	0.20	high- iC ₄ , C ₅ to C ₇ , CO ₂	14.26
Sample Cylinder EF4	All OK	0.63	high- C_3 , i C_4 , C_5 to C_7 low- C_1	18.10
Sample Cylinder EF5	All OK	0.23	high- iC ₄ , C ₅ to C ₇	13.76

Table 9. Summary of results from the tests of the Pitot and Bypass method conducted in November at the Powder Wash field site.

	Repeatability		Reproducibility	
	Components not Meeting Criteria	Max. Heating Value Deviation (Btu/scf)	Components Not Meeting Criteria	Max. Heating Value Deviation (Btu/scf)
Sample Cylinder PP1	No data available		No data available	
Sample Cylinder PP2*	All OK	0.18	high- C_6 , C_7	7.39
Sample Cylinder PP3 [†]	All OK	0.33	low- C ₃	0.64
Sample Cylinder PP4 [†]	iC ₄	3.28	low- iC ₄	3.92
Sample Cylinder PP5 [†]	All OK	0.85	low- C ₃	1.16

^{*90} second purge time prior to sample collection, †60 second purge time prior to sample collection.

3.2.4 Test Conditions – Repeat Tests

Due to the difficulties encountered with the analysis of the samples from the Powder Wash site, it was decided to repeat the tests of some of the methods. Repeat tests of the Fill-and-Empty, Helium Pop, and Pitot and Bypass methods were conducted on December 19, 2003 at the Powder Wash site by Questar personnel. Based on previous experience among members of the API Ch. 14.1 Working Group, these methods were expected to pass if performed correctly. The repeat tests also provided an opportunity to test these methods again under conditions in which all of the sampling equipment was insulated. Recall, as discussed in Section 3.2.2, that only the sample cylinder was insulated during the November tests. For the December tests, a second valve assembly (for use between the pipeline and the sample cylinder) was

kept in a heated storage container and was used to replace the assembly in use when its temperature dropped below the ambient temperature. Also, Questar personnel used one exposed-junction thermocouple to measure the surface temperature of the sample cylinders, rather than the tubing near the cylinder inlet, as was done in November. Other than these modifications, the procedures for the repeat tests were exactly identical to those used during the November tests.

Figure 16 shows the stability of the stream heating value and nitrogen content in the pipeline, measured at one-hour intervals over the course of several days around the time of testing. The nitrogen content remained fairly constant, but the heating value exhibited a regular fluctuation of about ± 25 Btu/scf. As was the case during the November tests, the gas stream temperature was very close to the HCDP, as would be expected for the flow just downstream of a separator station, and the temperature and heating value fluctuated in tandem. However, the period of the fluctuations is very long compared with the time interval during which the samples were being taken, and thus the composition was likely stable while the sampling was being performed.

As required by the proposed test protocol, the HCDP of the gas stream was measured immediately prior to collection of the gas samples and was determined to be 65°F. Since it was dark when the testing was completed, it was not possible to measure the HCDP again at the conclusion of the tests.

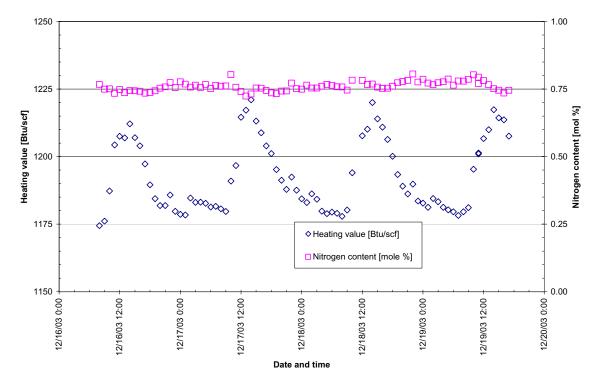


Figure 16. Long-term trends in stream heating value and nitrogen content around the time of the sampling tests conducted in December at the Powder Wash field site.

The flowing stream conditions and the temperatures of the sampling hardware, along with the gas stream and ambient temperatures, are plotted in Figure 17 and Figure 18 for the periods that the samples were taken. For these tests, the temperature of the sample cylinder was above the HCDP over almost the entire duration of the sample. This may be attributable to the use of insulation blankets around the cylinders and the fact that the valve assemblies were kept in hot storage until used. The sample probe

temperature, however, was below the HCDP, as in November. It is likely that the portion of the sample probe outside the pipe wall was still cooled by exposure to ambient conditions during the repeat tests.

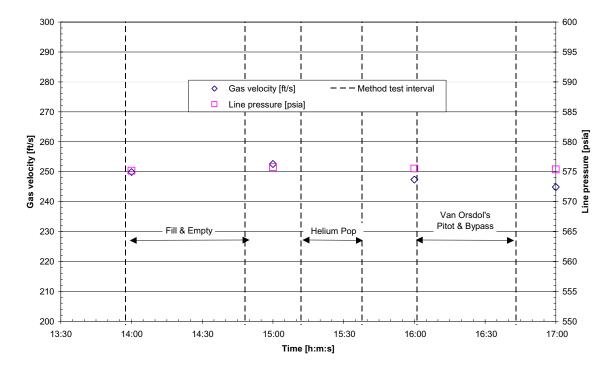


Figure 17. Flowing gas velocity and line pressure in the pipeline during the sampling tests conducted in December at the Powder Wash field site. Vertical dashed lines show intervals during which samples were taken by the various methods. Flow was in an 8" diameter pipe.

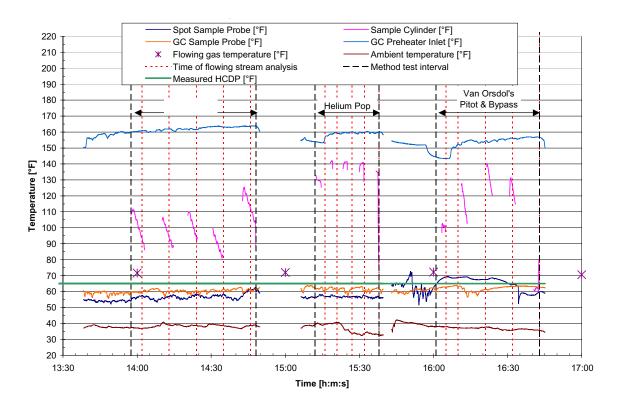


Figure 18. Equipment and gas temperatures during the sampling tests conducted in December 2003 at the Powder Wash field site. Black vertical lines with long dashes indicate intervals during which samples were drawn using the various methods. Red vertical lines with shorter dashed lines indicate times when GC analyses of the flowing stream were obtained.

3.2.5 Results – Repeat Tests

The results obtained from the repeat tests of the three sampling methods are summarized in Table 10 through Table 12, which are in the same format as those presented earlier. The procedures for analyzing the gas samples were exactly the same as those used for the November tests. The complete results of the analyses of each sample have been included in Appendix D.

Although all samples from the three methods met the repeatability criteria, at least one sample from each of the methods failed to meet one of the reproducibility requirements. For the Fill-and-Empty method, the reproducibility of the compositions was acceptable, but the heating value of one sample was greater than the 3 Btu/scf reproducibility limit set by the proposed test protocol. For the other two methods, the only reproducibility failures were high nitrogen content in some of the samples. The high nitrogen content may be the result of a small air leak that occurred at some point during the process. These results will be discussed in more detail in Section 3.3, where they will be compared to the results obtained from the other sampling tests.

Table 10. Summary of results from the retest of the Fill-and-Empty method conducted in December at the Powder Wash field site.

	Repeatability		Repro	ducibility
	Components not Meeting Criteria	Max. Heating Value Deviation (Btu/scf)	Components Not Meeting Criteria	Max. Heating Value Deviation (Btu/scf)
Sample Cylinder FE1	All OK	0.11	All OK	0.23
Sample Cylinder FE2	All OK	0.09	All OK	0.97
Sample Cylinder FE3	All OK	0.11	All OK	4.10
Sample Cylinder FE4	All OK	0.07	All OK	2.14
Sample Cylinder FE5	All OK	0.10	All OK	2.47

Table 11. Summary of results from the retest of the Helium Pop method conducted in December at the Powder Wash field site.

	Repeatability		Repro	ducibility
	Components not Meeting Criteria	Max. Heating Value Deviation (Btu/scf)	Components Not Meeting Criteria	Max. Heating Value Deviation (Btu/scf)
Sample Cylinder HP1	All OK	0.03	high- N ₂	0.05
Sample Cylinder HP2	All OK	0.08	high- N ₂	0.26
Sample Cylinder HP3	All OK	0.16	All OK	1.42
Sample Cylinder HP4	All OK	0.45	All OK	1.09
Sample Cylinder HP5	All OK	0.17	high- N ₂	2.15

Table 12. Summary of results from the retest of the Pitot and Bypass method conducted in December at the Powder Wash field site.

	Repeatability		Repro	ducibility
	Components not Meeting Criteria	Max. Heating Value Deviation (Btu/scf)	Components Not Meeting Criteria	Max. Heating Value Deviation (Btu/scf)
Sample Cylinder PP1*	All OK	0.08	high- N ₂	1.49
Sample Cylinder PP2*	All OK	0.34	All OK	1.10
Sample Cylinder PP3*	All OK	0.04	All OK	1.89
Sample Cylinder PP4*	All OK	0.03	All OK	0.33
Sample Cylinder PP5*	All OK	0.14	All OK	0.57

^{*90-}second purge time prior to sample collection.

3.3 Assessment of the Sampling Methods

The results from all of the sampling tests are summarized in Table 13. In this table, "Passed" means that the method met all of the requirements of the proposed test protocol, while "Acceptable" indicates that the method met most of the requirements, except for some minor deviations that are noted in the table. Methods that did not meet the requirements are listed as "Failed". Among the methods tested, two of the established GPA sampling methods (Fill-and-Empty and Helium Pop) produced representative samples of the gas stream under both optimum and adverse conditions. The Pitot and Bypass method, which was tested only under adverse conditions, was the only new method to meet the requirements of the proposed test protocol. The Controlled Rate Purge method passed the protocol requirements under optimum conditions at the MRF. The Controlled Rate Purge method and the High-Pressure Helium Displacement methods failed under adverse conditions at the Powder Wash site during November, but were not included in the December retests due to project constraints.

Table 13. Comparison of results from all sampling tests performed in this project.

I		an sampling tests periorined	1 3
Line Temperature	at least 32°F above HCDP	at HCDP	6°F to 8°F above HCDP
Ambient Temperature	at least 48°F above HCDP	at least 28°F below HCDP	at least 22°F below HCDP
Stream HCDP	below 37°F	69°F	65°F
Line Pressure	1009-1014 psia	578-582 psia	575-576 psia
Fill-and-Empty	Passed	no data available (all samples lost before air leak discovered)	Acceptable (heating value outside reproducibility limits on one sample)
Controlled-Rate Purge	Passed	Failed	Not tested
Helium Pop	Passed	Failed	Acceptable (N ₂ outside reproducibility limits on three samples)
Pitot and Bypass Method	Not tested	Failed	Acceptable (N ₂ outside reproducibility limits on one sample)
High-Pressure Helium Displacement Method	Not tested	Failed	Not tested
Modified Helium Pack Method	Not tested	Not tested	Not tested

From the comparisons shown in Table 13, it can be seen that the sampling conditions can affect how well a particular sampling method obtains a representative sample of the flowing gas stream. The Helium Pop method, which passed tests at the MRF, failed during the November field tests, but passed when it was retested in December with all equipment insulated from the ambient air. Likewise, the Pitot and Bypass method failed the November field tests, but provided acceptable samples in the December repeat tests. The likely explanation for the improvement in the repeat tests in both of these cases is that the sample lines and valves were kept at a higher temperature by the insulation and the practice of keeping the equipment in a heated container until use. Recall that although the sample cylinders themselves were insulated in both sets of tests, the valves and sample lines were only insulated during the December repeat tests. During the November tests, the portion of the sample probe outside the pipe wall was 13°F to 25°F below the HCDP, and only 10°F to 20°F above ambient temperature; during the December tests, the exposed portion of the probe was no more than 10°F below the HCDP, yet 20°F to 30°F above ambient temperature. This shift of the probe temperature toward the line temperature and away from the ambient temperature suggests that the insulation added to the sampling apparatus helped to keep the equipment warm and improved the quality of the samples.

The Controlled Rate Purge method and the High-Pressure Helium Displacement method were two other methods than failed under adverse conditions with no insulation of the sample lines and valves. Since these methods were not included in the December retests, it is not possible to draw any definite conclusions about how they might have performed if the sampling equipment had been insulated to keep equipment temperatures higher. However, the Controlled Rate Purge method was successful when tested under optimum conditions at the MRF. Based on the performance of the Helium Pop and Pitot and Bypass methods, it is possible that these two failed methods would also perform better under adverse conditions if all equipment were insulated. In summary, these results indicate that attention to the sampling apparatus temperature is an important factor in obtaining representative samples under adverse conditions with any method.

4.0 Conclusions

This report presents the results of experimental research to evaluate a proposed test protocol for verifying the performance of natural gas sampling methods. The primary goal of this testing was to evaluate the test protocol itself, and a secondary goal was to determine the ability of several new sampling methods to provide representative gas samples. The protocol was evaluated by using it to test some of the sampling methods currently found in GPA 2261 that are known to provide accurate results when performed correctly. In addition, several newly-proposed methods that are not currently included in the industry standards, but show potential as viable alternatives, were also tested. Sampling methods were judged based on repeatability and reproducibility criteria for both composition and heating value, as established by the proposed test protocol. The protocol is intended to serve as a means of assessing new gas sampling methods for the natural gas industry, and should facilitate the development of new and better gas sampling methods.

Testing of the methods was carried out under both optimum and adverse conditions. For the purposes of this report, "optimum" conditions were considered to be situations where both the pipeline and the ambient temperatures are both well above the hydrocarbon dew point (HCDP), and "adverse" conditions were situations in which the pipeline temperature is at or just above the HCDP, but the ambient temperature is below the HCDP. The tests under optimum conditions were performed at the SwRI Metering Research Facility, and the adverse condition tests were conducted at a Questar Pipeline metering station in Powder Wash, Colorado. Facilities and conditions at each site were carefully documented to support the conclusions in this report.

The sampling tests that were performed helped to identify difficulties with the procedure in the proposed test protocol, and to determine the practicality of the procedure and its ease of implementation in field settings. The key conclusions obtained from this investigation regarding the proposed test protocol are as follows:

- The acceptability criteria in the proposed test protocol appear to be appropriate to distinguish between sampling methods that are acceptable and unacceptable (i.e., methods that do or do not produce a representative sample of a flowing gas stream). Established sampling methods from GPA 2166, expected to pass the protocol criteria, did produce representative samples of the gas stream to within the required limits of the proposed test protocol.
- The requirements on the gas chromatographs used in the tests are rigorous, but more attention to GC calibration and stability may be needed, especially in applications where a portable GC is used in the field. The GC should be calibrated and used in a climate-controlled environment, or calibrated in the same environment in which it is used. Checking the GC calibration during and after tests may also be advisable.
- Air leaks in the analysis equipment were not found during preparations specified by the proposed test protocol. A revision to address this issue is suggested.
- Verifying the GC calibration gas at an independent lab, as required by the proposed test protocol, may not be necessary. Since the objective is to compare sample cylinder contents to the flowing stream, the validity of the comparison depends primarily on the repeatability of the GC.
- A way to simplify the dew point measurements required by the protocol should be considered. Problems commonly encountered in chilled mirror dew point measurements, including water vapor formation and inadequate ambient lighting, posed difficulties during the tests.

- Careful documentation is required during tests. Instruments that time-stamp data, such as flow meters, gas chromatographs, and data loggers must be synchronized to avoid errors in data comparisons.
- The proposed test protocol currently states that the chosen sampling location should have a steady flow rate and a stable composition. However, it does not specify the interval over which these quantities are to be monitored nor does it give limits of acceptability for flow rate variations. These should be addressed in the revision to the proposed protocol.
- To attain representative samples from streams near the HCDP, special attention should be given to the sampling equipment temperatures. For best results, an environmental chamber may be needed around the sampling apparatus. Recent tests with composite samplers at the Powder Wash site (Reference 3) indicate that the use of a chamber to keep sampling equipment warm can produce consistent and accurate samples of a gas stream near its dew point. Also, to ensure that the GC and spot sampling apparatus obtain identical samples, the sample delivery lines and probes should be heated and conditioned identically.
- The proposed test protocol does not currently address where the GC sample location should be relative to the spot sample location. A revision to address this is suggested. The revision should discuss the relative location (upstream or downstream) of the GC probe from the spot sample location, the distance from the sample location, and permitted pipe geometry.
- The protocol is currently being amended to specify test conditions by line temperature and HCDP, rather than by heating value; guidelines for both ambient and flowing gas temperatures during tests will now be included in the protocol.

Three GPA sampling methods (Fill-and-Empty, Controlled Rate Purge, and Helium Pop) and three proposed new sampling methods (Pitot and Bypass, High-Pressure Helium Displacement, and Modified Helium Pack) were tested. The key conclusions obtained from this investigation regarding the sampling methods are as follows:

- All of the established GPA sampling methods tested using the protocol produced representative samples of the gas stream under optimum conditions. The Fill-and-Empty and Helium Pop methods were also found to produce acceptable results when used correctly under adverse conditions.
- The Pitot and Bypass method, which was tested only under adverse conditions, was the only one of the three new methods to meet the requirements of the proposed test protocol.
- The Controlled Rate Purge method and the High-Pressure Helium Displacement methods failed under adverse conditions when the sample lines and valves were not insulated. These methods were not included in the field retests.
- Both the Helium Pop and the Pitot and Bypass methods failed in adverse conditions when the sample lines and valves were not insulated, but subsequently passed when they were retested with fully insulated sampling equipment. This result demonstrates that attention to the sampling apparatus temperature is an important factor in obtaining representative samples under adverse conditions.
- The Modified Helium Pack method could not be tested, due to equipment failure related to the cold conditions at the field site.

5.0 References

- 1. <u>Manual of Petroleum Measurement Standards, Chapter 14 Natural Gas Fluids Measurement, Section 1 Collecting and Handling of Natural Gas Samples for Custody Transfer, American Petroleum Institute, Washington, D.C., USA, 5th edition, June 2001.</u>
- 2. <u>Obtaining Natural Gas Samples for Analysis by Gas Chromatography,</u> GPA Standard 2166-86, Gas Processors Association, Tulsa, Oklahoma, USA, 1986.
- 3. Kelner, E., Sparks, C. R., and Behring, K. A., <u>Metering Research Facility Program, Natural Gas Sample Collection and Handling Phase III: Experimental Investigation of Gas Sampling Techniques and Equipment, Gas Research Institute, Des Plaines, Illinois, USA, August 2002.</u>

This page is intentionally blank.

Appendix A

Proposed Performance Verification Test Protocol

This page is intentionally blank.

API MPMS Chapter 14.1

New Spot or Composite Sample Method Performance Verification Procedure

Testing will be limited to a single-phase gas stream at or above its hydrocarbon dew point (HCDP). Multi-phase fluid sampling is not within the scope of this procedure. Laboratory practices described in this document should not be interpreted to be required procedures for normal sampling and analysis.

Procedure

- 1. The same chromatograph used to analyze the sample stream is to be used to analyze the spot or composite samples to eliminate the error of using different chromatographs. It is preferable to use chromatographs for testing that are capable of producing an extended analysis (C_{9+}) accurate within the API Chapter 14.1 guidelines for repeatability and reproducibility. The use of analyzers limited to a C_{6+} output may provide test results that indicate that the sampling method is acceptable for the application tested; however, method approval from such results should not be extrapolated to include applications where a more extended analysis is required.
- 2. Establish that the online or portable chromatograph and sample delivery system complies with API Chapter 14.1. See Appendix (E) for repeatability and reproducibility criteria and inspection checklist. The same calibration method and calibration standard is to be used for all chromatographs used for testing.
- 3. Calibration standards must be prepared in accordance with the requirements in API Chapter 14 Section 1 (paragraph 14.1.16), maintained in accordance with the requirements in GPA 2198-98, and verified by a laboratory independent of the blender. Verification of the calibration standard must comply with API Chapter 14.1 Appendix E repeatability and reproducibility criteria.
- 4. Establish that the complete sampling system (chromatograph, cylinders, tubing, etc.) is clean and free of any contaminants prior to calibrating and testing. Verify that the sample delivery system and chromatograph are clean by analyzing a sample of ultra-high purity (UHP) helium. Verify the cleanliness of the sample cylinders by charging them with 50 psig of UHP helium, heating to 125 degrees F for 2-4 hrs, and then analyzing the helium. No peaks should be produced during these procedures.
- 5. If the sample method is tested under controlled laboratory conditions (as in 5a below), performance verification is recommended on multiple gas blends. If the method is tested on a single flowing gas composition at an established metering location (as in 5b below), the results may not apply to a broad spectrum of gas compositions.
 - a) Verify the method on at least two and preferably three gas blends that represent a broad spectrum of gas compositions commonly encountered in gas gathering and transportation

- operations. For example, a three-gas test might use blends that produce gross heating values of 1000 BTU, 1175 BTU, and 1350 BTU.
- b) Select a location for sampling that has a steady flow rate and a stable gas composition. Verification of stability will be established before sampling is conducted. Stability is defined as the repeatability of consecutive analyses as defined by API Chapter 14.1 Appendix E.

6. Determine the HCDP using the following steps:

- a) Use the Bureau of Mines dew scope with a NIST-traceable thermometer and a video attachment.
- b) Heat the sample line to the Bureau of Mines scope to 20-50 degrees F above the HCDP.
- c) Utilize two technicians to determine the dew point. Each technician shall run a minimum of three dew points to establish repeatability.
- d) The determined dew point must agree within two (2) degrees F to eliminate uncertainty.
- e) The dew point is to be checked before and after the sampling procedure tests.

7. Determine the composition of the flowing stream using the following steps:

- a) Verify and document the stability of the composition of the flowing gas stream using a portable or on-line chromatograph.
- b) The chromatograph is to be analyzing the stream during sampling procedures.
- c) The chromatograph software will be required to archive and Time- and Date-stamp the chromatograms, composition, and the corresponding BTU. The methods and calibration chromatograms used for each testing procedure shall be saved.
- 8. Also capture and record sufficient data to demonstrate the stability of the dynamic flowing conditions of the stream during the sampling tests.

9. Conduct sampling method using the following steps:

a) A minimum of five (5) samples shall be obtained for each method tested.

10. Analysis Requirements

- a) Each cylinder shall be heated to 20–50 degrees F above the HCDP for a period of 2–4 hours before analyzing.
- b) Each cylinder is to be analyzed a minimum of three times to establish repeatability as defined by API Chapter 14.1 Appendix E.

11. Data Requirements

a) The data shall be in tabular form and in a format that is easy to read and understand.

- b) The data shall be available for public review.
- c) The spot sample analysis report shall reference the corresponding online or portable gas analysis report.
- d) On-line chromatograph data for comparison with composite samples shall be averaged for the same time period as the composite samples.
- 12. Verification of sampling procedure: Sample heating values shall agree within the greater of the tolerances described below or those defined by API Chapter 14.1 Appendix E.
 - a) Review the data to ensure that the accuracy of the spot or composite sample method complies with the repeatability and reproducibility for each component as stated in API Chapter 14.1 Appendix (E).
 - b) The three successive analyses of each test cylinder must repeat within one (1) BTU per cubic foot
 - c) Each test cylinder must reproduce within three (3) BTU per cubic foot of the online or portable chromatograph.
 - d) Analyses of each composite sample cylinder must reproduce within (3) BTU per cubic foot of the average of the online chromatograph for that sampling period.

The following addition to Step 5 of the test protocol was submitted for ballot in June 2003:

5. c) The protocol is intended to evaluate the performance of new or proposed sampling systems and procedures under ideal conditions and under conditions when only the best current methods will succeed. For example, in a case where two gases are used during the evaluation, the lean gas may be used to verify good performance when the gas is far from its hydrocarbon dew point (HCDP) and ambient temperatures (real or induced) are higher than the flowing temperature of the stream. The richer gas, during the same evaluation, would be used to evaluate the performance of the new or proposed sampling system and procedure when the ambient temperature is colder than the flowing temperature of the stream and the measured hydrocarbon dew point of the stream, and the flowing stream is at a temperature very near its HCDP.

To fully confirm the suitability of new or proposed sampling systems and procedures, it is recommended that the flowing stream during one phase of the evaluation program be within 5°F of its' measured HCDP and that the ambient temperature (actual or induced) be at least 20°F colder than the flowing temperature of that stream.

Record the Following Information

Record test data on a spreadsheet and provide as much additional information as possible, including copies of analyses from labs.

- Description of the sample method
- Description of the test used to evaluate the sample method
- Date of test
- Location of the Test
- Personnel conducting the tests
- Personnel witnessing the tests
- Pipeline Pressure
- Pipeline Size
- Piping Configuration (Upstream and Downstream)
- Sample probe style and description
- Sketch or photo of the piping scheme for the test site
- Description or photo of the test method equipment and physical installation used in test
- Description of the flowing gas stream, i.e., well head, separator, distribution system, meter run, gathering system, etc.
- Ambient Temperature
- Pipeline Flowing Temperature
- Sampling Apparatus Temperature for sample method and reference analyzer. As a minimum, include the temperature at the sample probe and at the exit point of the sample delivery system.
- Description of temperature control equipment (i.e. insulation, heater, steam)
- Hydrocarbon Dew Point
- Cylinder Style
- Cylinder Size
- Sampler style (if applicable) and description
- Timed or Proportional to flow
- Sample volume size
- Approximate elevation of the test location

GC Description

- Last calibrated and how, relative to test data
- Provide records for calibrations performed immediately before, during and after the testing, including response factors and repeatability data

Appendix B

Procedures for New Sampling Methods

This page is intentionally blank.

High Pressure Helium Displacement Method

Proposed by Eric Fritz, Natural Gas Pipeline Company of America

Sample Cylinder Preparation

- 1. Sample cylinders must be thoroughly cleaned before samples are taken.
- 2. Momentarily purge the sample cylinder with helium, and then fill the cylinder to the minimum pressures according to the table below.

Sample Source	Helium Pre-Fill Pressure (psia)			
Pressure	Cylinder Size			
(PSIA)	150-cc	300-сс	500-сс	1000-cc
30	84	79	77	76
40	95	90	87	86
50	106	100	98	96
60	118	111	108	106
70	129	122	119	116
80	140	132	129	127
90	152	143	139	137
100	163	153	150	147
200	276	260	254	249
300	389	366	358	351
400	502	473	462	453
500	615	579	566	555
600	728	686	670	657
700	841	792	774	759
800	954	899	878	861
900	1067	1005	982	963
1000	1180	1112	1086	1065
1100	1293	1218	1190	1167
1200	1406	1325	1294	1269
1300	1519	1431	1398	1371
1400	1632	1538	1502	1473
1500	1745	1644	1606	1575

Note: Assume length from sample probe tip to sample inlet valve of 12" x 1/4". Do not exceed pressure rating of sample cylinder.

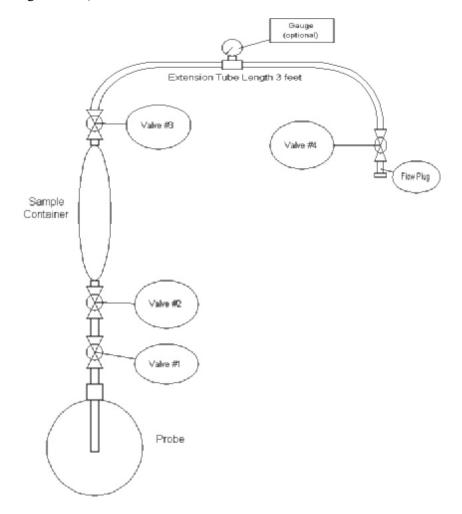
3. Remove sample cylinder from Helium source and check for leaks by immersion of the valves in water or by use of a commercial leak detection solution. Plug valves (if female) or cap valves (if male).

Sampling Method

Note: Insure that the temperature of the sample cylinder exceeds the temperature of the sample source. A minimum of 10°F is recommended. If not, an unrepresentative sample may be obtained.

1. Open sampling source valve (Valve 1) and thoroughly blow out any accumulated material. Close valve at sampling point.

2. Install sample cylinder as shown in the Figure below. The cylinder is preferred to be in the vertical position but may be horizontal to facilitate close connection of the sample cylinder to the probe outlet (if using an angled valve).

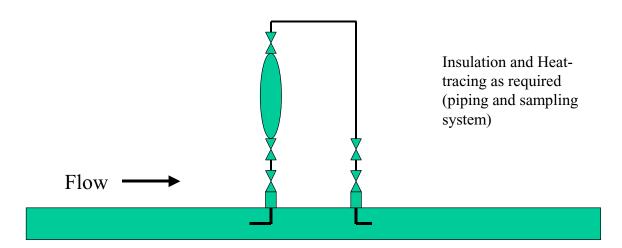


- 3. Install a 3-ft. piece of 1/4" diameter tubing and the extension tube valve (Valve 4) as shown.
- 4. With all valves closed, open the sample cylinder inlet valve (Valve 2) to allow Helium to fill the connection between the sample cylinder and sampling point valve.
- 5. Open the sampling point valve (Valve 1) to allow Helium to flow (back flush) through the sample probe and into the pipeline. The pressure in the cylinder will equalize with the pressure of the sample source.
- 6. Open the sample cylinder outlet valve (Valve 3) to fully open position.
- 7. Open the extension tube valve (Valve 4) fully. A ½-turn valve works best.

8. Flow in this manner for the time specified in the following table.

Flow Plug		Cylind	er Size	
Drill Size	150-cc	300-сс	500-cc	1000-cc
76 (0.0200")	35 sec	75 sec	115 sec	230 sec
79 (0.0145")	70 sec	135 sec	210 sec	450 sec

- 9. Close the sample valves in the following order: extension tube valve (Valve 4), cylinder outlet valve (Valve 3), cylinder inlet valve (Valve 2), and sampling point valve (Valve 1).
- 10. Open extension tube valve (Valve 4) to allow extension tube pressure to bleed off. Remove the extension tube from the sample cylinder.
- 11. Source pressure will exist in the close-coupled connection between the sample point valve and the cylinder inlet valve. Carefully remove the sample cylinder from the probe by bleeding off pressure, as the short coupling is unscrewed.
- 12. Check sample cylinder for leaks by immersion of the valves in water or by use of a commercial leak detection solution. Plug valves (if female) or cap valves (if male).



This system would include a Pitot tube inside the meter run facing upstream, followed at the appropriate distance by a Pitot tube facing downstream. Both tubes would be connected to external sampling equipment via vertical couplings welded onto the top of horizontal piping.

On the outlet of the upstream coupling would be a full opening, permanently mounted valve (<u>full opening</u> ball valves for example – not the typical 1/8" diameter passage valves on current cylinders). Close coupled to that valve, in the vertical, would be a sample cylinder with similar full opening valves on its' inlet and outlet. From the sample cylinder outlet valve, tubing would return to the pipe and connect immediately to a full opening valve mounted on the downstream coupling.

All external (to the piping) materials would be insulated and/or heated. All metal in the sample system except the couplings would be stainless steel.

If the flowing temperature of the stream is above the hydrocarbon dew point temperature, no heat will be required – only adequate insulation. If the flowing temperature were at the dew point temperature, heat would also be required. This may limit the utility of this proposal in remote locations without a source of heat. However, even in remote locations we might be able to rig up a safe, temporary heating system, perhaps powered by a vehicle.

To prepare the system for service, a clean cylinder with a high-pressure helium blanket (higher than line pressure) would be installed. Note that a low-pressure helium blanket might be ok, but I'm concerned about the initial fill when a new cylinder is brought into service.

Except when sampling, all valves would be closed.

To purge the cylinder and begin the process of sampling, the clean, helium-pressurized cylinder would be

placed into service by opening the full opening valve on the downstream tap, then the valve on the upstream tap, then the cylinder <u>inlet</u> valve, then the cylinder outlet valve.

To trap a spot sample, the downstream tap valve would be closed, then the sample cylinder outlet valve. Next the cylinder inlet valve would be closed, then the upstream tap valve. The cylinder would then be removed from service, capped, checked for leaks, and then shipped to a lab for analysis.

A fresh helium pressurized cylinder would then be installed, with all valves closed until a new sample is needed.

Modified Helium Pack Spot Gas Sampling Method

Proposed by R. Mark Haefele, BP

Apparatus required:

- Pipe thread on the sample cylinder valve that mates with the pipe thread on the sample probe valve,
- Vacuum pump, and
- Pipe thread on the vacuum pump connection that mates with the pipe thread on the sample cylinder valve

Procedure:

- 1. Evacuate the subject sample cylinder
- 2. Fill the sample cylinder with ultra-high purity (UHP) helium to a pressure at least 100 psig above the anticipated line pressure.
- 3. Loosely thread the sample cylinder directly into the sample valve mounted above the sample probe.
- 4. Slowly open the bottom valve on the sample cylinder, bleeding UHP helium into the void between the sample cylinder and the sample probe valve while tightening the connection.
- 5. Fully open the sample probe valve, equalizing the pressure on the helium pack in the sample cylinder with the line pressure, and clearing the sample probe with UHP helium.
- 6. Close the sample probe valve.
- 7. Evacuate the helium pack from the sample probe valve and the sample cylinder through the top valve on the sample cylinder.
- 8. Close the top valve on the sample cylinder.
- 9. Open the sample probe valve, filling the sample cylinder to line pressure.
- 10. Close the bottom sample cylinder valve.
- 11. Close the sample probe valve.
- 12. Disconnect the sample cylinder from the sample probe valve.
- 13. Test cylinder valves for "bubble tight" seal using a bucket of water or leak check liquid.
- 14. Plug and seal valve ports, tag the cylinder, secure and transport in accordance with company safety requirements.

Purposes:

- Collect a representative spot sample of gas without emitting greenhouse gas to the atmosphere
- Clear the sample probe without emitting greenhouse gas to the atmosphere
- Eliminate the phase change problems associated with the purge Fill-and-Empty procedure

Appendix C

GC Setup and Calibration Results

This page is intentionally blank.

C.1 Laboratory Inspection Checklist

This section presents the API MPMS Chapter 14.1, Appendix E laboratory inspection checklist that was used to survey the chromatograph and sample delivery systems at the MRF and Powder Wash field sites. This checklist was used to verify that the analysis systems at these sites complied, as mandated by the proposed test protocol, with the requirements of API Chapter 14.1. Results of the survey at both locations are recorded below.

Laboratory

Date of Survey

Survey Conducted By

SwRI MRF	Questar API
July 10, 2003	November 9, 2003
Darin L. George	Darin L. George

Sample Handling & Conditioning

Are sample cylinders heated?

If sample cylinders are heated, to what temperature?

Is the sample cylinder temperature monitored?

Is the sample heated for at least 2 hours?

Is time monitored for sample cylinder heating?

What is the length of time used for heating sample cylinders? (# hours)

Are samples taken immediately from heater to analyzer if manually transferred?

What method is used to insulate heated sample cylinders during analysis?

Insulated Blanket

Heated Cabinet

Other (Specify)

Comments

No (see comments)	Yes
	125°F
Ambient monitored	Temperature of storage room monitored electronically (see comments)
	Yes
	No
	At least 12 hours (overnight)
	See comments
	No
	Yes
Ambient temperature 40°F above dew point; heating not required	Cylinder is placed in a room heated to 125°F and left overnight. Cylinders are connected to a manifold within the room, and samples are drawn through the manifold to a GC outside the room.

Physical Facility

Is the analyzer room heated?
Is the analyzer room air-conditioned?
Comments

No	Yes
No	Yes
Analyzer is installed outside, as designed. Columns are in insulated ovens	

Filters, Connections, and Hardware

Filters, Connections, and Hardware		
Are filters used between sample and analyzer?	Yes	When liquids are suspected in sample
Type:	NuPro SS-4TF-15	
Size:	15 μm sintered filter	20 μm filter
Replacement Interval:	No regular interval	
What are the size, length and material of sample line and fittings?	1/8" diameter stainless steel tubing, 51 to 60" long; SS fittings	1/8" stainless steel tubing, 10 ft long; SS fittings
Are connections, lines, and hardware between sample cylinder and analyzer insulated?	No (ambient temperature 40°F above dew point during use)	Yes
Are connections, lines & hardware between sample cylinder and analyzer heated?	No (ambient temperature 40°F above dew point during use)	Yes
Sample loop size:	Loop 1: 0.1648 cc Loop 2: 0.7524 cc	Variable injector
Comments		Analyzer regulator is heated to 200°F

Injection System

Is the sample system a vacuum injection system?

Is the sample system a purge injection system?

If purge injection system, is there backpressure?

Can the purge rate be read or measured?

What is the purge rate?

Comments

No	Yes
Yes	Yes
Yes	Yes
No (see comments)	No (see comments)
	400 cc/min
Back pressure can be monitored; pressure is 85 psig, within specs	Analyzer typically uses vacuum injection, then purge injection. Back pressure adjustable but not measurable; flow rate measurable.

Analyzer

What is the analyzer brand?

What is the analyzer model?

What is the analyzer's serial number?

Is this an isothermal run?

If "YES," record temperature in °C.

If "NO," secure a copy of the temperature program.

Are the columns configured per GPA 2261?

If "NO," list the configuration.

Integration method:

Peak height

Area

Data logging method:

Manual

Electronic

Highest carbon number component analyzed .

1S:

Calibration schedule is:

Analysis frequency is:

Daniel	Varian
Daniel 2350 GC	Varian 4900 Quad GC
384073	4910070
Yes	Yes
82°C	Channel A: 103°C Channel B: 87°C
Yes	Yes
No	No
Yes	Yes
No	No
Yes	Yes (Star software)
C ₉ +	C ₉ +
Daily	Daily
5-minute intervals	Weekly

Carrier Gas

What is used as the carrier gas?

What is the purity of the carrier gas?

Is the carrier gas pressure monitored?

Is the carrier gas flow rate monitored?

If yes, carrier gas flow rate in cc/minute:

Is a carrier gas drier used?

If yes, type of drier material used:

Replacement interval of carrier gas drier material:

Helium	Helium
99.999%	99.999%
Yes	Yes
Yes	No
0.55 to 0.65 sccm	
No	No (dry environment)

Calibration Standard Gas

Manufacturer of calibration standard

Is calibration standard age less than a year old?

If "NO", list the date blended

Is the calibration standard heated continuously?

If no, list the length of time heated before use:

To what temperature is the calibration standard heated?

Is an insulation blanket or heated cabinet used for the calibration standard?

Can the cylinder pressure of the calibration standard be monitored?

If yes, record the pressure in PSIG before and after each test.

Does the lab have calibration standards required for the test program?

Is the hydrocarbon dew point for the calibration standard available?

If yes, hydrocarbon dew point:

Has or could the calibration standard ever been exposed to a temperature below the hydrocarbon dew point?

Comments

	D.C.C.D
Scott Specialty Gas	DCG Partnership
Yes	Yes
No	Yes
Not heated (see comments)	
Not heated (see comments)	125°F
No	Yes (heated room)
Yes	Typically yes, though the standard used for these tests was not monitored
95 psig	
Yes	Yes
Yes	Yes
Cricondentherm = 27°F	Cricondentherm = 84.9°F
No	Yes (see comment)
Calibration standard is kept in a climate-controlled room at 70°F; transfer lines to GC are heated to 120°F. The dew point of the standard is computed before use to confirm that the room temperature is not below dew point.	Standard was placed in a heated room at 125°F for two weeks before use.

Calculation

Are the component constants used in accordance with the latest GPA 2145?

If "NO," what constants are used?

Can the constants be verified?

Are the calculations performed in accordance with the latest version of GPA 2172?

Other methods used:

Values for C_6 + or other heavy fraction:

 C_6

 C_6 +

 \mathbf{C}_7

 C_7 +

Other (Specify)

Composition of fraction:

 C_6

 \mathbf{C}_7

 C_8 +

Other (Specify)

No	No
GPA 2145-95	GPA 2145-00
Yes	Yes
Yes (GPA 2172-96)	Yes (GPA 2172-96)
None	None
As given in GPA 2145	As given in GPA 2145
As given in GPA 2145	As given in GPA 2145
C ₈ as given in GPA 2145; all heavier components assigned values for C ₉	C ₈ as given in GPA 2145; all heavier components assigned values for C ₉
	,
As measured	As measured
As measured	As measured
C ₈ as measured	C ₈ as measured
Co as incasarca	C ₈ as measured

Quality Control Program

Does a Quality Control Program exist?

Can a copy of the Quality Control Program be obtained?

Comments

Yes	Yes
No (currently under revision)	Not available
QC program includes statistical process control, checks of standards	QC program includes regular audits, tests of helium blank samples, different standards, records kept for 2 years

NOTE: Rating by Team

Documentation

Secured area counts and response factors?

Secured chromatograms and results?

Secured copy of analysis report for calibration standards?

Secured relative density?

Secured HV - saturated and unsaturated, both real and ideal?

Secured mol% both normalized and unnormalized?

Secured starting and ending pressures for both lab's calibration standard and audit group's standards?

Yes	Response factors only
Yes	Yes
Yes	Yes
Yes	Specific gravity recorded
Real heating values only	Real heating values only
Yes	Yes
Pressure recorded for lab standard (no audit standard used)	No (not available for lab standard, no audit standard used)

C.2 GC Calibrations

The following sections present the details of the chromatograph calibrations that were performed for the tests conducted at the MRF, the Powder Wash field site, and the repeat tests at the Powder Wash field site.

C.2.1 MRF GC

The MRF GC was calibrated on a 1,030 Btu/scf gas. Figure C-1 is a plot of the calculated dew point curve for the calibration gas. This plot confirms that it is not necessary to heat the calibration gas, since the gas is kept in a climate controlled room which maintains the gas at a temperature at least 50°F above the computed cricondentherm. The fidelity plots for the two columns in the GC are shown in Figure C-2 and Figure C-3. The relative response factors for both columns follow a linear trend, as expected.

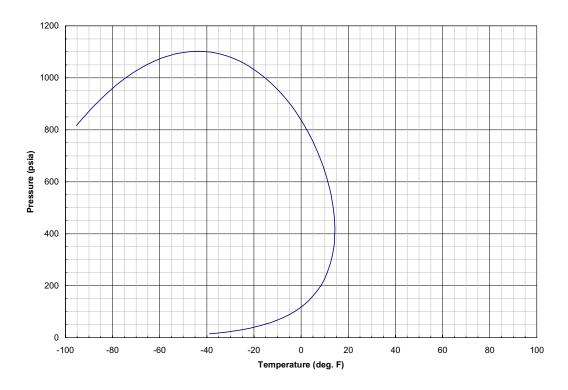


Figure C-1. Dew point curve for gas used to calibrate the Daniel 2350 GC at the MRF. Curve computed from SRK equation of state.

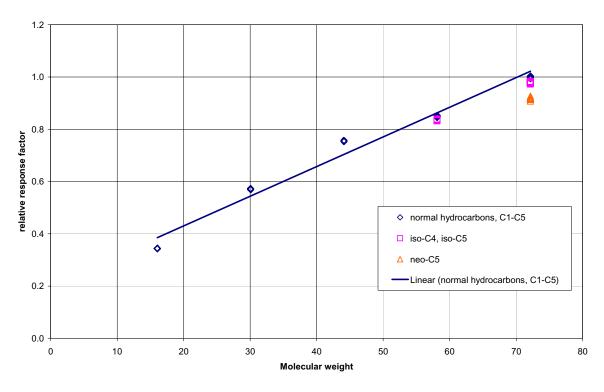


Figure C-2. Fidelity plot for column A of the MRF Daniel 2350 GC. June 2003 calibration runs on Scott gas #XL002396.

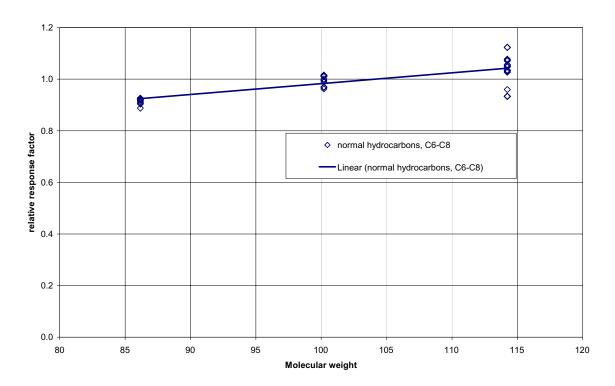


Figure C-3. Fidelity plot for column B of the MRF Daniel 2350 GC. June 2003 calibration runs on Scott gas #XL002396.

C.2.2 Powder Wash GC

The portable GC at the Powder Wash site was calibrated on a 1,200 Btu/scf gas. Figure C-4 is a plot of the calculated dew point curve for the calibration gas. The gas was maintained at 125°F, which was 40°F above the computed cricondentherm. The fidelity plots for the two columns in the GC are shown in Figure C-5 and Figure C-6. The relative response factors for column A are linear, but not for column B. As a further check on the GC operation, the GC was calibrated on a second gas and showed linear response factors for both columns. The fidelity plots for the second calibration are shown in Figure C-7 and Figure C-8. The acceptable calibration on the second gas suggests that there were no problems with the operation of the GC, but rather that the stated composition of the first gas blend was not correct.

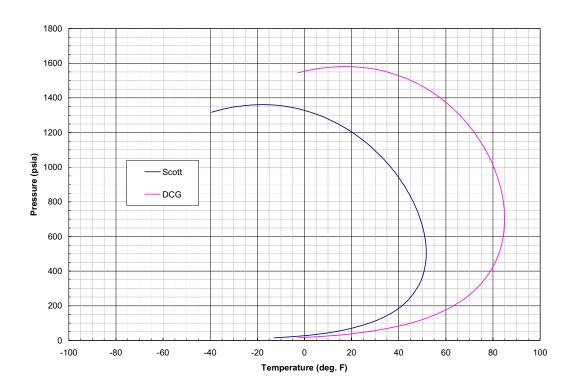


Figure C-4. Dew point curves for gases used to calibrate the Varian CP-4900 GC at the Powder Wash site. Curves computed from SRK equation of state.

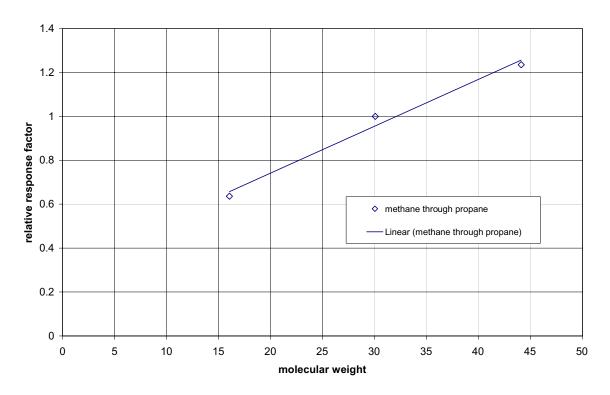


Figure C-5. Fidelity plot for column A of the Varian CP-4900 GC at the Powder Wash site. November 11 calibration run on DCG gas #22933AW.

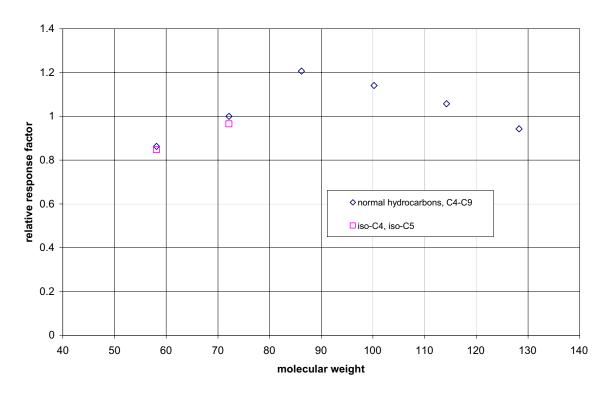


Figure C-6. Fidelity plot for column B of the Varian CP-4900 GC at the Powder Wash site. November 11 calibration run on DCG gas #22933AW.

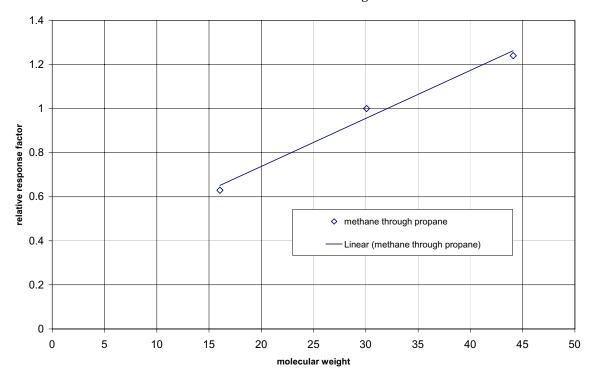


Figure C-7. Fidelity plot for column A of the Varian CP-4900 GC at the Powder Wash site. November 12 calibration run on Scott gas #ALM051559.

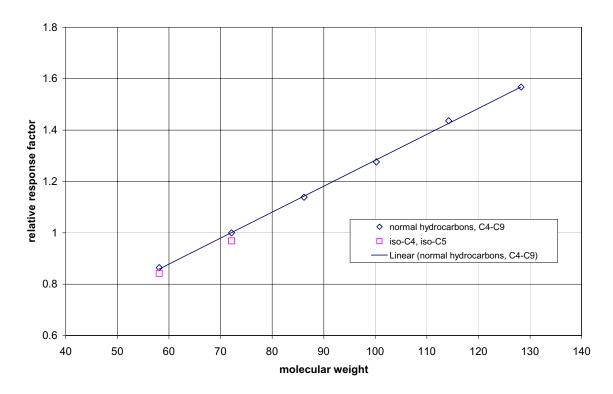


Figure C-8. Fidelity plot for column B of the Varian CP-4900 GC at the Powder Wash site. November 12 calibration run on Scott gas #ALM051559.

C.2.3 Powder Wash GC - Repeat Tests

The portable GC at the Powder Wash site used for the retests was calibrated on the same 1,200 Btu/scf gas as used previously. The fidelity plots for the two columns in the GC are shown in Figure C-9 and Figure C-10. As in the calibration for the November tests, the relative response factors for column A are linear, but not for column B.

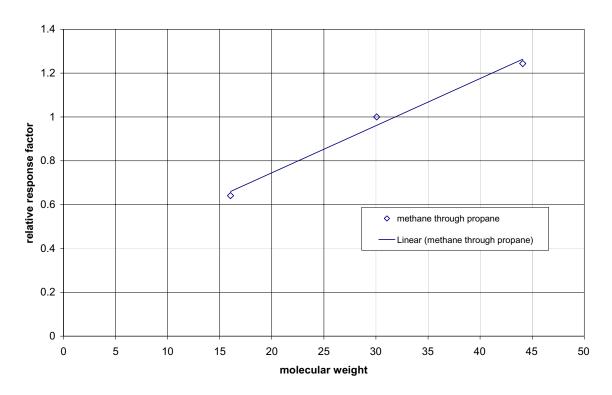


Figure C-9. Fidelity plot for column A of the Varian CP-4900 GC at the Powder Wash site.

December 18 calibration run on DCG gas #22933AW.

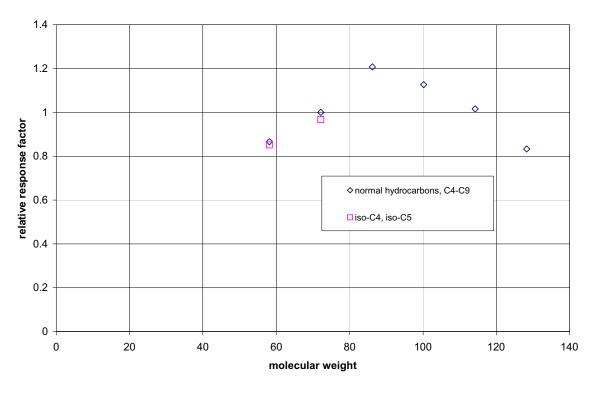


Figure C-10. Fidelity plot for column B of the Varian CP-4900 GC at the Powder Wash site.

December 18 calibration run on DCG gas #22933AW.

Appendix D

Detailed Test Results

The following tables compare the analyzed compositions of each sample with an analysis of the flowing gas stream taken at approximately the same time as the sample. The contents of each sample cylinder were analyzed three times to assess the repeatability of the sample method. The results of each cylinder analysis were compared to the flowing stream analysis to assess the ability of the sampling method to reproduce the stream composition.

This page is intentionally blank.

Table D-1. Detailed results from MRF sampling tests, June 18, 2003: Fill-and-Empty method.

alysis-1 (Mor%) alysis-2 (Mor%) alysis-3 (Mor%) assalve (Mor%)	Date 6/18/2003	Sample Time 13:17 - 13:20	Methana 92.212402 92.208473 92.210625 0.00	289621 38994 38994 38994 0.00			1.072227 0 1.072227 0 1.072543 0 1.072385 0 0.00		0.00	0.000	9	0.017408 0.01667 0.01667 0.00	0.018637 0.018637 0.0186 0.00 0.00	0.009688 0.0106784 0.010678 0.00		골 = = =
Repeatable / Universe Paniss) Repeatable / Acceptable / Repeatable / Acceptable / Max. Absolute Orevaion [Mod's] Reproducible / Criteria (± Mol's) Reproducible / Acceptable /	6/18/2003	13:15	752 7ES 92.15296 0.02 0.63 7ES	4.388204 0.00 0.13 7ES	0.00 0.00 0.13 7ES	76S 805647 000 76S	7.073966 0.00 0.13 7.55	0.00 0.00 0.00 7ES	7ES 0.00 7ES 7ES	000 000 000 000 VES	000 000 000 VES	758 0009614 0.04 758	0.022916 0.00 0.00 7ES	000 000 000 7ES	7ES 0.00 0.00 7ES 7ES	1.00 YES 1056.5625 0.05 3.00 YES
Sample FEZ Sample Gifter GC Analysis - I Morifs) Eample Bottle GC Analysis - I Morifs) Sample Bottle GC Analysis - I Morifs) Mac. Absolute Desiston-Successive (Morifs) Mac. Absolute Desiston-Coreal (Morifs) Repeatability - Critical E. Morifs Repeatability - Critical E. Morifs Repeatability - Critical E. Morifs Mac. Absolute Oession (Morifs) Reconsideration contact of Morifs) Reconsideration contact of Morifs Reconsideration Constant (Morifs) Reconsideration Constant (Morifs) Reconstant (Morifs) R	Date 6/18/2003 6/18/2003	13:28 - 13:38 13:38 - 13:38	Mathana 92.205053 92.205050 0.00 0.00 0.52 YES 92.19136 0.01	Ethana 4.393944 4.393944 4.39372 0.00 0.10 YES 4.39977 4.39977 1.13	CCC2 1.094031 1.093449 0.00 0.00 0.00 0.10 0.10 0.10 0.10 0.1	Nanagan F 0.827852 1, 0.8263 1, 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	Propane 18 1.074487 0 1.074485 0 0.00 0.00 0.10 0.10 0.10 0.10 0.10 0.					Nespentans 0.017336 0.01718 0.00 0.00 0.00 7ES 0.00 100 100 100 100	n-Hazana 0.01881 0.018492 0.00 0.00 0.00 0.02 VES 0.023088	0.000000000000000000000000000000000000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Hv dry IBu/scf) 1065/79489 1065.01294 1065.05437 0.15 0.15 1.00 YES 1098.92744 3.00
Reproducibility Acceptable?			YES	ÇES CES	£83	ÆS	YES	YES		YES	YES	YES	YES	ÆS	YES	YES
Sample FE3 Sample Peter (Analysis) (MoRS) Sample Bottle GC Analysis (MoRS) Max. Alsolute Destinication (MoRS) Max. Alsolute Destinication (MoRS) Repeatablity Criteria (E-MorS) Repeatablity Criteria (E-MorS) Max. Absolute Destinic (MoRS) Max. Absolute Destinic (MoRS) Reproducibity Criteria (E-MorS) Reproducibity Criteria (E-MorS) Reproducibity Criteria (E-MorS)	Date 6/18/2003 6/18/2003	Sample Time Mathema 13.48 - 13.54 92.200.54		4.394969 4.3924659 4.392563 0.00 0.00 0.00 7.ES 7.ES 7.ES 7.ES 7.ES	COZ 10000000 11000000 11000000 11000000 1100000 1100000 1100000 1100000 1100000 1100000 110000 110000 110000 110000 110000 110000 110000 110000 1100000 110000 110000 110000 110000 110000 110000 110000 110000 1100000 110000 110000 110000 110000 110000 110000 110000 110000 1100000 110000 110000 110000 110000 110000 110000 110000 110000 1100000 110000 110000 110000 110000 110000 110000 110000 110000 1100000 110000 110000 110000 110000 110000 110000 110000 110000 1100000 110000 110000 110000 110000 110000 110000 110000 110000 1100000 110000 110000 110000 110000 110000 110000 110000 110000 1100000 1100000 110000 110000 110000 110000 110000 110000 110000 1100000 110000 110000 110000 110000 110000 110000 110000 110000 1100000 110000 110000 110000 110000 110000 110000 110000 110000 110000 110000 110000 110000 110000 110000 110000 110000 110000 1100000 110000 110000 110000 110000 110000 110000 110000 110000 1100000 1100000 1100000 1100000 1100000 1100000 1100000 1100000 11000000	Ningen F 0.000963 1 0.000963 1 0.000964 1 0.00 0.00 0.00 0.00 0.00 0.00 0.00	Propers Is 1.074673 0 1.074085 0 1.074085 0 0.00 0.00 0.10 0.10 0.13 0.13 0.13			Isopertane Pertane Oct Oct	Pertain P-Pertain P-Pertai	Neopentane 0.0017477 0.0017488 0.000 0.000 YES 0.005516 0.000 0.000	0.01858 0.01868 0.018478 0.018478 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.01306 0.01306 0.010758 0.00 0.00 7ES 0.00 0.00 0.00	0.000 0.000 0.000 0.00 0.00 0.00 0.00	He dry (Burket) 1065 (B40342 1065 (B40342 1065 (B403467 1065 (B403467 1060 (B40347 1060 (B403467 1060 (B4047 1060 (B4047 1060 (B4047 1060 (B4047 1060 (B4047 1060 (B4047 1
Sample FEL Sample Pel Sample Bottle GC Analysis NortS) Sample Bottle GC Analysis NortS) Nea, Also the Gottle GC Analysis NortS) Max. Also the Devision Securosance (Ind'N, Max. Also the Devision Consense (Ind'N, Max. Also the Devision Concern MortS) Repeatablity Criteria (E. MortS) Repeatablity Acceptable (Ind'N, Max. Also the Devision (Ind'N, Max. Also th	Date 6/18/2003 6/18/2003	15-58 - 14:02 92.209601 19:58 - 14:02 92.209601 92.201997 0.011 0.01 0.052 14:00 92.20427 0.01 0.01		Ethans 4.39329 4.39329 0.00 0.10 YES 4.387126 0.01	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	805233 805233 805533 8056333 805634 7 FES 805647 9 000	Popens Is 1.07334 0 1.073495 0 0.00 0.00 0.10 YES 1.073843 0			0.000000000000000000000000000000000000	0.037301 0.037301 0.037305 0.037795 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	Department Pertain Neopertains O(0.0034 O(0.7246 O(0.7	0.000 0.0018487 0.000 0.000 0.002 0.002 0.002 0.002 0.000 0.000	P-Heptrane P-Octame H 00/1382 0,000282 0,00/1712 0,000395 0,00/1712 0,000395 0,000 0,000 1,000 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0,000	0.000088 0.000386 0.000386 0.000 0.00 0.00 0.00 0.00 0.00	Hr dry (Brusch) 1066,699023 1066,629503 106,62623 0.19 1.00 YES 1056,624688 1056,624688
Reproducibility Acceptable? Sample FES Sample FES Sample Bottle (CAndyteir-) (MolS) Sample Bottle (CAndyteir-) (MolS) Max. Absorbe Destition Canada (MolS) Repeatablity Criteria (E. MolS)	Date 6/18/2003 6/18/2003	Sangle Time Methons 1470 - 14:12 82.20:408 92.20:408 0.00 0.00 0.62 7.63 14:10 92.1976 0.01 0.01 0.01 0.03 7.63 14:10 92.1976 0.01		YES TENANG 1 20090 1 100 0.00 0.00 0.00 0.00 0.00 0.00		C S M S M	이외보다 의	95 D D		2 0 ± 0 0 0	YES (1976) 1	YES Neopertans 0.017147 0.0077138 0.007743 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	YES 0.018783 0.0018415 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.		7ES 1000209 0.00 0.00 0.00 0.00 0.00 0.00 0.0	YES H by [Bused] 105.66984 105.69894 105.69894 10.0 0.10 0.10 1.00 YES 100 YES

Table D-2. Detailed results from MRF sampling tests, June 18, 2003: Controlled Rate Purge method.

105 64002 1065 64002 1065 7107 0.24 0.24 0.03 1.00 YES 1066 48157 0.77 3.00 YES	Mospertaina In-Heavane In-Heaptene In-Catterine In-Heavane	Hv dry (Burker) 1066 624289 1066 621949 0.05 0.05 1.00 YES 1086 536278 0.87 3.00 YES	1065 89281 1065 89281 1065 133445 1065 143433 0.63 1.00 YES 100 YES 100 YES 100 YES 100 YES 100 YES	1006.36(9)6 1006.36(9)6 1006.26(9)4 1006.78(9)4 0.70 1.00 1.00 1.00 1.00 1.00 0.73 1.00 0.73 1.00 0.73 1.00 0.73 1.00 0.73 1.00 0.73 1.00 0.73 1.00 0.73 1.00 0.73 1.00 0.73 1.00 0.73 1.00 0.73 0.73 0.73 0.73 0.73 0.73 0.73 0
0.0000234 0.0000234 0.000034 0.000 0.00 0.00 0.00 0.00 0.	0.000091 0.00071 0.00071 0.000 0.00 0.00 0.00 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000487 0.000487 0.000681 0.000681 0.000 0.00 0.00 0.00 0.00 0.00 0.00 0	0.0002 0.00042 0.000289 0.000289 0.000 0.00 0.00 0.00 0.00 0.00 0.00 0
0.00913 0.001319 0.001319 0.00 0.00 0.00 7ES 7ES 0.00 0.00	0.000000000000000000000000000000000000	0.009999999999999999999999999999999999	0.009057 0.0030757 0.002475 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	0.00 SEA VES
0.018788 0.018783 0.01878 0.000 0.00 0.00 0.00 0.00 0.00 0.00	n-Hexana 0.01847 0.0180421 0.01816 0.002 0.02 0.02 0.02 0.02 0.02 0.03 0.03	0.016695 0.016695 0.00 0.00 0.00 0.00 0.02 YES 0.0124045 0.014	n-Haxana 0.018563 0.03005 0.03005 0.011 0.011 0.02311 0.014 VES	0.003443 0.003443 0.013689 0.013689 0.011 0.012629 0.011 0.014
Neopentane 0.017659 0.017687 0.017687 0.00 0.00 0.00 7ES 0.01 0.01 0.01	0.016813 0.016813 0.014378 0.00 0.00 7.55 7.55 0.031005 0.02 0.02	Neopentane 0.017002 0.016851 0.010 0.00 0.00 0.01 0.01 0.01 0.01	Neopertana 00/7019 00/5984 00/2984 000 000 000 000 000 000 000	Microportana b-Husana In-Highland In-Octana III- 8 0077478 0.003643 00.4628 0.00002 III- 8 007723 0.018889 0.00599 0.00009 0.00 0.01 0.01 0.01 0.00 0.00 0.01 0.01 0.01 7 0.02988 0.0298 0.0000 0.00 0.01 0.01 0.01 0.01 0.01 0.01 0.04 VES YES YES YES YES YES YES 0.000 0.01 0.01 0.01 0.04 VES YES YES YES YES YES YES 0.000 0.01 0.01 0.01 0.04
n-Pertana 0.036933 0.0377 0.0378 0.00 0.00 0.02 YES 0.00 0.00 0.00 0.00 0.00 0.00	0.037676 0.0376376 0.0376376 0.030 0.00 0.00 0.00 0.00 0.00 0.00 0.	0.037381 0.037381 0.037463 0.037627 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	n-Partana P 0.037504 0.037464 0.037492 0.000 0.00 0.00 0.00 0.00 0.00 0.00 0	0.03780 0.03780 0.03780 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0
0.04178 0.04178 0.042261 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	Sopertana O 042314 O 042314 O 042539 O 000 O 002	0.041822 0.041827 0.042345 0.00 0.00 0.00 0.02 VES 0.042512 0.00 0.00 0.00	topertana topertana topertana topertana topera topera	0.042399 0.0042399 0.0042399 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0
0.000000000000000000000000000000000000	0.168937 0.168937 0.00 0.00 0.00 0.02 0.02 0.02 0.02 0.0	ABUtana 0.170066 0.168951 0.00 0.00 0.02 YES 0.168903 0.00 0.00 0.00 0.00	hButana 0.170198 0.169273 0.170046 0.00 0.00 0.02 YES 0.168784 0.00 0.00	
Isobutano 0.110872 0.110872 0.110872 0.011244 0.00		0.111221 0.111221 0.111041 0.00 0.00 0.00 7ES 7ES 0.11085 0.00 0.00	111432 0.111432 0.111216 0.00 0.00 0.00 7ES 0.01075 0.00 0.00	1000 000 000 000 000 000 000 000 000 00
Propare 1.0730/7 1.0730/2 0.00 0.00 0.10 YES 1.073634 0.00 0.00 0.00 0.13 YES	Popare 1.072789 1.07269 0.00 0.00 0.10 YES 1.072865 0.00 0.00 0.13	Propare 1.072832 1.072832 1.072832 0.00 0.00 0.10 YES 1.073049 0.00 0.00	Proparie 1,072895 1,072129 0,00 0,10 0,10 0,10 1,072123 1,072123 1,072123 1,072123 1,072123 1,072123 1,072123 1,072123 1,072123 1,072123	Propare 1.072365 1.072865 0.00 0.10 2.10 2.10 2.10 0.00 0.00 0.00
Nanogen 0.627949 0.827462 0.00 0.00 1.00 7.65 7.65 0.00 0.00 0.00 0.00	Narogen 0.827166 0.82716 0.00 0.00 7ES 0.82765 0.00 0.00 0.00	Ninogen 0.626163 0.626142 0.606142 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	Ninogen 0.600393 0.627043 0.627043 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	Nitrogen 0.802875 0.802817 0.8027866 0.00 0.00 0.00 0.00 0.00 0.00
CO2 1.083147 1.083181 0.00 0.00 0.10 YES 1.092343 0.00 0.13 YES	C02 1.090862 1.0903131 1.091308 0.00 0.10 0.10 0.10 0.10 0.10 0.10 0.	0.00 0.00 0.00 0.00 0.10 0.10 0.10 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	C02 1.092916 1.092454 1.092454 0.00 0.10 0.10 0.10 0.10 0.10 0.10 0.1	000 000 010 000 010 010 010 010 010 010
Ethana 4.391447 4.386758 4.390499 0.00 0.10 YES 7.387389 0.00 0.00 YES 7.387389 0.00 0.13 YES	Ethana 4.386292 4.386796 1.00 0.01 0.01 7ES 4.38478 0.01 0.01 7ES	Ethana 4.38836 4.3887124 0.00 0.00 0.10 7ES 4.382753 0.01 0.01	Ethana 4.388145 4.388145 4.387454 0.00 0.00 7ES 4.380719 0.01 0.01 0.01	Ethana 4.389174 4.389271 0.00 0.10 7ES 4.387346 0.01 0.01
	Mathana 92.2110286 92.2110286 92.221909 0.01 0.01 0.52 YES 92.186249 0.04 0.03	Methans 92.213986 92.214378 92.214378 0.00 0.00 0.02 YES 92.196081 0.02 0.02	Methans 9.2.2106 9.2.20465 0.01 0.01 0.01 7ES 7ES 92.20466 0.01 0.01 0.01	Methans 82.194412 92.208785 92.208785 0.02 0.52 7ES 92.201523 0.01
Bample Time Methans 14.40 - 14.45 92.20836 92.20836 0.00 0.00 14.40 92.10838 14.40 92.10838 0.63 14.40 92.10728 0.63	Serropia Timos Methanos 1453 - 1457 82.211464 82.221095 82.221096 0.011 0.017 14:55 21:05.249 0.027 14:55 21:05.249 0.037 0.04	15.00 - 15.07 15.00 - 15.07 15.05	Sample Time 15:11 - 15:13 15:10	Sample Time Muthana 16:16 - 16:19 9.2 (34412) 92.20(3705) 0.012 0.02 0.02 0.02 0.02 0.02 0.02 0.0
Date 8/18/2003 6/18/2003	Date 6/18/2003 6/18/2003	6/18/2003 6/18/2003	Date 6/18/2003 6/18/2003	Date 8/18/2003 6/18/2003
Sample CRI Sample Bottle GC Analysis - Maris Max. Absolute Devision-Careal Maris Repeatablity Criteria It Maris Repeatablity Acceptable? Max. Absolute Devision (Maris Max. Absolute Devision (Maris Max. Absolute Devision (Maris Reproducibity Acceptable? Reproducibity Acceptable?	Sample CRZ Sample Bottle GC Anatysia-1 [Motis] [8 Sample Bottle GC Anatysia-2 [Motis] Sample Bottle GC Anatysia-2 [Motis] Sample Bottle GC Anatysia-2 [Motis] [Max. Absolute Devision-Careal [Motis] [Repeated by Christo Busine Christo Busine Government of the Motis] [Motis Busine Busine Government of the Motis Busine Busine Busine Busine Government [Motis] [Max. Absolute Devision [Motis]] [Max. Absolute Devision [Motis]] [Max. Absolute Devision [Motis]]	Sample CR3 Sample Bottle GC Analysis Maris Sample Bottle GC Analysis Maris Sample Bottle GC Analysis Maris Mac. Alsolute Devision-Carea Maris Repeated by Constron-Carea Maris Repeated by Acceptable? Repeated by Acceptable? Research Process GC Analysis Maris Max. Alsolute Devision Maris Reproducibility Acceptable? Reproducibility Criteria E. Maris Reproducibility Criteria E. Maris Reproducibility Criteria E. Maris Reproducibility Acceptable?	Sample CINA Surple Dattle GC-Analysis-2 (Mark) Sample Battle GC-Analysis-2 (Mark) Sample Battle GC-Analysis-2 (Mark) Max. Alsolute Devision-Clausecosine (Mark) Repeatablity Criterie it Mark) Repeatablity Acceptable GC-Analysis (Mark) Max. Absolute Overston-Clause (Mark) Repeatablity Acceptable GC-Analysis (Mark) Reproducibity Acceptable? Reproducibity Acceptable?	Sample CES Sample Bottle GC Analysis - I Motis) Sample Bottle GC Analysis - I Motis) Sample Bottle GC Analysis - I Motis) Max. Absolute Devision-Careal Motis) Repeatable Constructor-Careal Motis) Repeatable Citeria to Motis) Repeatable Citeria to Motis Repeatable Citeria to Motis Repeatable Control to Motis Repeatable Acceptable Max. Absolute Devision (Motis)

Table D-3. Detailed results from MRF sampling tests, June 18, 2003: Helium Pop method.

dry (Burbach) 566,698(2)2 566,698(2)2 566,704(8) 50.07 50.07 50.07 50.08 50.08 50.08 50.08 50.08 50.08 50.08 50.08 50.08 50.08 50.08 50.08 50.08 50.08 50.08	(Brusco) 697144 667144 662364 689707 1.04 1.00 1.00 1.00 1.00 1.00 1.00 1.00	Municol 8605 9605 9605 9605 9605 7	(Buvsct) 942773 942773 942773 953027 103 103 103 103 103 103 103 103 103 103	88005 86005 86005 77451 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
3555	444 444 444 444 444 444 444 444 444 44	Hwdy (Busket) 1056,796805 1056,794888 1066,794888 1067,794888 1068,794888 1068,794888 1068,794888 1068,794888	Hvdy (Bu/ss 1066 842773 1066 873027 1066 873027 106 0.03 1.00 YES 1080 3.00 YES	He day (Bauvoct 1068,006005 1065,89827 1065,892451 0.21 0.021 1.00 YES 1056,638306 0.84 3.00 YES
0.00028 0.00028 0.00 0.00 0.00 0.00 0.00	0.000038 0.000473 0.000 0.00 0.00 0.00 0.00 0.00 0.00 0	Octane 000078 000239 0002 000 000 000 000 000 000 000 000 0	0.000538 0.0000237 0.00071 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	00000000000000000000000000000000000000
0.000000000000000000000000000000000000	0.000000000000000000000000000000000000	Heptana 0.009486 0.010302 0.010302 0.00 0.00 0.00 0.00 0.00 0.00 7.ES	0.00138 0.001488 0.001488 0.001047 0.00 0.00 0.00 0.00 0.00 0.00	0.01781 0.01781 0.01781 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.
0.018831 0.018831 0.01833 0.00 0.00 0.00 0.02 YES 0.00 0.00	Respectation A-Housing A-Hoptisms A-Housing A-Hoptisms A-Housing A-Hoptisms A-Ho	0.018786 0.003495 0.003495 0.003495 0.003495 0.000 0.00 0.00 0.00 0.00 0.00 0.00 0	Neopertana n-Neosna n-Neoprana n-Neo	n-Hazana 0.018921 0.018481 0.00 0.00 0.02 YES 0.022786 0.00 0.00 0.00
P-Purtana Nappartana 0.037621 0.016356 0.027621 0.016356 0.007 0.07726 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.01 0.00 0.01 0.00 0.01 0.00 0.01 0.00 0.01	Neopertans 0.017382 0.017381 0.00 0.00 7ES 0.01 0.01 0.01 0.01	Neppertans Nepertans Nepertans Nepertans Nepertans Nepertans Nepertan	Neopentane 0.017109 0.017348 0.017348 0.00 0.00 0.01 0.01 0.01	Neopentane 0017806 0017805 000 000 7ES 002946 000 7ES
n-Pertana 0.037621 0.037478 0.03 0.00 0.00 0.02 YES 0.03779 0.00 0.00	0.037176 0.037176 0.03707 0.00 0.00 0.02 VES 0.03771 0.00 0.00	-Partans 0.039651 0.03751 0.00 0.00 0.02 VES 0.037975 0.00 0.00 0.00	0.037549 0.037549 0.037545 0.037545 0.00 0.00 0.02 YES 0.037808 0.00 0.00	n-Pertana 0.037459 0.037431 0.037633 0.00 0.00 0.02 VES 0.00 0.00 0.00 0.00 0.00
Isopertana 0.042177 0.041893 0.000 0.000 0.002 VES 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	Inspirator Portators Outside	0.04236 0.04236 0.04248 0.017248 0.00 0.00 0.02 7ES 0.00 0.00 0.00 0.00 0.00 0.00	Industriane Pulidana Industriane Pulidana Industriane Indust	Isopertans O.042234 O.042245 O.00 O.00
		NEW Part Part Part Part Part Part Part Part	0.16893 0.16893 0.16893 0.00 0.00 0.00 0.02 YES 0.00 0.00 0.00 0.00	0.169824 0.169824 0.169344 0.00 0.00 0.02 VES 0.169072 0.169072
Iobulano n-Bitana Iobulano			0.111374 0.111374 0.111374 0.00 0.00 7ES 7ES 0.00 0.00	0.111387 0.111387 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.
Propane 1.078049 1.075623 1.075685 0.00 0.10 VES 0.00 0.13 VES	Propered 1.074546 1.074546 0.00 0.00 0.10 YES YES YES YES	Propana 1.075406 1.075752 1.075766 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	Propara 1.07588 1.07574 1.075783 0.00 0.10 0.00 0.10 0.00 0.13 VES 0.13 0.00 0.13 0.00	Properer 1.079581 1.079781 0.00 0.10 0.10 0.00 0.10 0.00 0.00 0.
Ningan 0.034769 1.0837308 1.0837308 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	Nitrogen 0.632166 0.633634 0.00 0.00 0.00 1.625 1.625 0.01 0.01 0.04	Nitrogen 0.823/346 0.823/346 0.00 0.00 7 ES 7 ES	Ntrogen 0.82730 0.824994 0.00 0.00 0.00 7ES 0.00 0.00 0.00	Ninogen 0.692/521 0.893/64 0.00 0.00 0.00 7ES 0.82/566 0.00 0.00 0.00 0.00
000 000 010 000 010 010 010 010 010 010	C02 1.092317 1.092538 1.092538 0.00 0.00 0.10 YES 1.093604 0.13 YES	C02 1.002167 1.002762 1.002762 0.00 0.00 0.10 7.ES 7.ES 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	C02 1.093627 1.092709 1.092709 0.00 0.10 YES 0.00 0.13 YES	000 0.00 0.00 0.00 0.00 0.00 0.00 0.00
Ethana 4.396396 4.39482 4.395866 0.00 0.00 0.00 0.00 0.00 0.00 0.00	Ethana 4.394761 4.394200 4.394200 0.00 0.00 7.55 7.55 7.55 7.55 7.55 7.	Ethana 4.38738 4.386699 0.00 0.00 7.55 4.386138 0.00 0.00 7.55 7.55 7.55 7.55 7.55 7.55	Ethans 4.399026 4.395978 0.00 0.00 0.10 7ES 7ES 7ES 7ES	Ethana 4,396059 4,396059 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0
	Mathana 92.196789 92.200286 0.00 0.00 0.52 YES 92.178388 0.02 0.63	Methana 82.2185989 82.2185198 0.011 0.011 0.022 VES 7ES 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.0	Methans 82.197.243 92.200652 92.200677 0.00 0.01 0.52 755 92.178428 0.03 0.03 0.03 0.03 755 755 755 755 755 755 755 755 755 75	Methans 92 198612 92 198485 92 168797 0.01 0.62 YES 92 178429 0.02 0.63
Sangia Tima Mathana 11.02 - 11.04 92.199527 20.19698 20.19698 20.19698 10.59 92.18218 10.59 92.18218 10.59 92.18218 20.1	11.05 - 11.06 11.05 - 11.06	Bample Time 11:12 - 11:13 11:08	Bample Time Methans Ethans 11:16 - 11:18 52:09243 4 3498928 92.20562 4 398389 0.000 0.01 0.00 0.01 0.02 0.10 0.01 0.02 11:14 92:178429 (2091) 0.03 0.03 11:14 92:178429 (2091) 0.03 0.03	Sample Time 11:10 - 11:10 11:14
B/18/2003	Date 8/18/2003 E/18/2003	6/18/2003 6/18/2003	6/18/2003 6/18/2003 6/18/2003	6/18/2003
Sample HPT Sample Bottle (CANatysisch MoNS) Sample Bottle (CAnatysisch MoNS) Sample Bottle (CAnatysisch MoNS) Max. Absolute Devision-Successe [MoNS) Repeatability Criteria [L MoNS) Represibility Acceptable Reproducibility Acceptable Reproducibility Acceptable Reproducibility Acceptable Reproducibility Acceptable Reproducibility Acceptable Reproducibility Acceptable	Sample Britle GC Analysisc Mot Kill Earnigh Britle GC Analysisc Mot Kill Earnigh Britle GC Analysisc Mot Kill Max. Absolute Devisitor Excessive [Mat Kill Max. Absolute Devisitor (Analysis) Repeatablity Criticis IE Mot Kill Repeatablity Criticis IE Mot Kill Max. Absolute Devisitor (Mot Kill Repeatablity Criticis IE Mot Kill Repeatablity Acceptable) Max. Absolute Devisitor (Mot Kill Reproducibility Acceptable)	Sample HP3 Sample Bottle GC Analysis of MotSi Sample Bottle GC Analysis of MotSi Sample Bottle GC Analysis of MotSi Max Absolute Devision-Cureoi (MotSi) Max Absolute Devision-Cureoi (MotSi) Max Absolute Devision-Cureoi (MotSi) Max Absolute Devision (MotSi) Max Absolute Devision (MotSi) Reproducibity Acceptable? Reproducibity Acceptable? Reproducibity Acceptable?	Sample HP4 Sample Bottle GC Analysisc Mo15/3 Sample Bottle GC Analysisc Mo15/3 Sample Bottle GC Analysisc Mo15/3 Max. Absolute Devision-Cuccasing [Mo15/3] Repeatablity Critical E Mo15/3 Reproducibility Acceptable? Reproducibility Acceptable?	Sample PHTS Sample Bottle GC Analysical (MorSa) Sample Bottle GC Analysical (MorSa) Sample Bottle GC Analysical (MorSa) Max. Absolute Devisitor-Careal (MorSa) Repeatable Py Critical & MorSa) Repeatable Py Critical & MorSa) Repeatable Py Critical & MorSa) Max. Absolute Devisitor (MorSa) Max. Absolute Devisitor (MorSa) Max. Absolute Devisitor (MorSa) Representable Oriental & MorSa) Representable Oriental & MorSa)

Table D-4. Detailed results from Powder Wash sampling tests, November 10, 2003: Controlled Rate Purge method.

Sample CR1 Sample GR4 CC Analysis MorSs 11.00.2004 16 Sample Bottle CC Analysis MorSs Sample Bottle CC Analysis MorSs Max. Absolute Deviation Successive MorNs Max. Absolute Deviation Successive MorNs Max. Absolute Deviation Deviation MorSs Repostability Citeria MorNs	11/10/2004	Sample Time 15:00 - 15:01		Methans 84,3922 84,3715 0.02 0.02 0.62		40723 40734 40796 0.01 0.10	2	1.1376 1.1376 1.1405 1.000 0.00	2	9	0.178 0.178 0.178 0.00 0.00 0.00	0.000 0.000 0.000 0.000 0.000	0.032 0.034 0.034 0.00 0.00	0.00	0.438 0.438 0.4384 0.000 0.000	PoooB	1199 (Burser) 1199 (B34 1199 (B34 0 (B5 0 (B5 100 100	Hv sat [Btu/scf) 1178 6214 1178 4936 1160.3974 0.84 0.84
Repartating Acceptable Process GC Analysis (Mat/S) Max. Absolute Davistion (Mat/S) Reproducibility Criteria is Mat/S) Reproducibility Acceptable?	11/10/2003	15.04	0.6714 0.04 0.04 NO	0.34 0.63 7ES	768 0.02 0.05 768	40171 0.05 7ES	0.022 0.03 7ES		0.04 VES VES	0.2467 0.03 7.65	0.1329 0.05 0.06 NO	0.0782 0.014 7ES	0.0216 0.01 0.04 YES	VES 4000	0.4368 1000 YES	100 B 00 A	YES 1191.1378 8.78 3.00 NO	7ES 1171.7004 8.64 3.00 NO
Sample CR2 Sample Bottle GC Analysisc1 [Marits] Sample Bottle GC Analysisc2 [Marits] Sample Bottle GC Analysisc2 [Marits] Max. Absolute Deviation-Successive [Marits] Max. Absolute Deviation-Denail [Milits] Conventi	11/10/2004	Sample Time 15.08 - 15.11	nitrogen	тефат	ethane	a un boud	so-butane n	n-butane 1-	i pentane	- neutran	haxanea	haptamas	25 Elli	monanes	8	塁	Hr dry (Blurisci)	Hv sat (Btu/sct)
reprotective Process of Caralysis (Nortical Mars. Aboutte Derastion (Nortical Mars. Aboutte Derastion (Nortical Mars.) Reproducibility Criteria (± Modifical Mars.)	11/10/2003	15.08	0.88	84,7329 84,73 0,63	7.0826	40194 4.02 0.13	0.93	1.0884	20 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.24	0.1346 0.004	0.008	0.002	0000	0.4301	0 8 8 8	1190,7341 1190,73 3.00	1171.3035 1171.30 3.00
Sample OCS Sample Bottle GC Analysis-1 (MaRS) Bangie Bottle GC Analysis-2 (MaRS) Bangie Bottle GC Analysis-2 (MaRS) Max. Absolute Deviation-Duccessive (Mark) Max. Absolute Deviation-Deviation-Duccessive (Mark) Repeatability Acceptable Repeatability Acceptable Reproducibility Acceptable? Reproducibility Acceptable?	0ate 11/10/2004 11/10/2003	Sample Time 16:16 - 16:18 16:17	nitrogen 0.8344 0.9068 0.008 0.005 0.005 0.005 0.005 0.005 0.006 0.006	methane 84,5288 84,5288 84,5288 0.03 0.03 0.62 YES 84,6252 0.03 0.03	ethane 1 7.0981 7.0985 0.00 0.00 0.16 7.1622 0.07 0.26 YES	A 4.0397 4.0397 4.0394 0.00 0.00 0.10 0.10 0.10 0.13 0.13 0.13	0.9423 0.9423 0.9423 0.942 0.00 0.00 0.02 7 YES 0.947 0.00 0.00 0.00	1.1108 1.1108 1.1108 1.1108 1.000 1.00 1.	1	n-pertiane 0.2630 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	hexanes 0.1641 0.1663 0.000 0.000 0.000 0.003 0.004 VES 0.004	heptanes 0.1023 0.1047 0.1056 0.00 0.00 0.02 VES 0.0051 0.0051 0.0051	00000000000000000000000000000000000000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.02 0.4326 0.4328 0.02 0.00 0.00 0.00 0.00 0.00 0.00 0.	S 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1196.847 1196.847 1196.847 1196.871 0.25 1.00 YES 1190.5689 5.04 3.00	Hr sat (Budoct) 1175,9946 1175,9946 1175,6798 1175,6798 1170,777 1100 1100 1100 1100 1100 1100
Sample CRA Sample Bettle CCA Analysis MotSA 11/10/2004 15 Sample Bettle CCA Analysis MotSA 11/10/2004 15 Sample Bettle CCA Analysis MotSA Max. Absolute Deviation Successive [MotSA Max. Absolute Deviation Sonial MotSA Repeatablity Citeria H. MotSA Repeatablity Citeria H. MotSA Max. Absolute Deviation MotSA Reproducibility citeria H. MotSA Reproducibility Citeria H. MotSA Reproducibility Citeria H. MotSA Reproducibility Acceptable?	11/10/2004 11/10/2004 11/10/2003	16.22 - 16.26 16.22 - 16.26 16.22	0.0000 0.0000 0.0000 0.000 0.00 0.00 0	84,6327 84,6287 84,6287 0.00 0.01 0.62 YES 84,9187 0.39 0.39	athana 7.1302 7.1402 7.1402 0.00 0.00 0.18 7.0904 0.05 7.0904 0.05	4.0619 4.0619 4.0635 0.00 0.10 YES 0.25 0.13 0.13	0.9407 0.09427 0.09427 0.09427 0.000	1.0974 1.0974 1.0974 1.0975 1.0975 1.0975 1.0975 1.0975 1.0975 1.0982 1.	0.3676 0.3676 0.3678 0.3678 0.00 0.00 0.00 7ES 0.3544 0.00 7ES	0.2538 0.2538 0.2538 0.2538 0.000 0.000 0.000 0.001 0.001 0.001	0.1524 0.1524 0.1526 0.000 0.00 0.00 0.00 0.00 0.00 0.00 0	0.0914 0.0923 0.0923 0.092 0.00 0.02 0.02 0.02 0.02 0.02 0.0	0.0238 0.0242 0.0242 0.00 0.00 0.00 0.00 0.01 0.019 0.014 VES	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.4508 0.4508 0.4508 0.000 0.000 0.000 0.000 0.000 0.000 0.000	H 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1190 8847 1190 8847 1190 8847 1190 8847 1190 884 1100 12 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.	H vari (Bu/scd) 1174.3916 1174.3916 1174.4956
Sample OSS Sample Battle CO Analysis-1 [Mol75] Sample Battle CO Analysis-2 [Mol75] Sample Battle CO Analysis-3 [Mol75] Max. Absolute Deviation-Successive [Mol76] Repeatablity Criteria it Mol76] Repeatablity Criteria it Mol76] Recounted by Acceptable Control (Mol75) Max. Absolute Deviation [Mol76] Recounted by Acceptable Control (Mol76) Reproducablity Acceptable Control (Mol76) Reproducablity Acceptable Control (Mol76) Reproducablity Acceptable Control (Mol76)	0ste 5s 11./10/2004 15	Sample Time 15:23 - 15:31 15:31	nitrogen 0.8539 0.8539 0.00 0.00 1.00 1.00 1.00 0.00 0.00 0.0	methane 84,4235 84,4705 0.02 0.02 VES 84,8282 0.35 0.35	ethane 1 7,1144 7,1159 0,00 0,00 0,18 7,1026 0,02 0,02 0,02 0,02	Properties 18 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	190-butane In 0.9614 0.9644 0.09644 0.000	1,1108 1,1108 1,1108 1,000 0,000 1,0089 1,0089 1,0089 1,0089 1,0089 1,0089 1,0089 1,0089 1,0089 1,008	0.3707 0.3707 0.3706 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	Prentane 0.2535 0.2545 0.00 0.00 0.02 VES 0.02 0.02 0.02 VES 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.0	0.1449 0.1449 0.146 0.000 0.000 0.002 0.1306 0.002 0.002	heptanes 0.0059 0.0064 0.00 0.00 0.00 0.00 VES VES 0.0751 0.00 0.00 VES	octanes 00225 00225 0.000 0.00 0.002 VES 0.0173 0.0173 0.0173	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0.4579 0.458 0.000 0.000 0.000 0.4366 0.4366 0.4366 0.004 7ES	\$000B8B\$\$000B	1194 (198) 1194 (198) 1194 (208) 1194 (208) 0.50 0.84 1.00 VES 1198 (216) 6.61 3.00 80	Hr sat (Bushect) 1174,7852 1174,8974 1176,33 0.49 0.62 1.00 YES 1.00 YES 6.50 3.00

Table D-5. Detailed results from Powder Wash sampling tests, November 10, 2003: Helium Pop method.

Sample HPT Data Sample Sample Sample Bottle GC Analysis-1 [Marks] 11/10/2003 167. Sample Bottle GC Analysis-2 [Marks] Sample Bottle GC Analysis-2 [Marks] Sample Bottle GC Analysis-2 [Marks]	11/10/2009	Sample Time 15:54 - 15:56	0.959 0.959 0.9582 0.9722	methans 84,6484 84,6324 84,6267	7.069 7.069 7.065	-	9	1.0747 1.0753 1.0753		0.2416 0.2416 0.2417	0.1402 0.1405 0.1402	0.0824 0.0823 0.0825	0.0208 0.0248	30000000000000000000000000000000000000	0.4582	¥0008	1189.4113 1189.4113 1189.4208 1189.5854	Hv sat (Btu/sct) 1170,0032 1170,0125 1170,1744
Max. Absolute Lovation-Successive [Mays.] Max. Absolute Deviation-Ownel [Mol%] Repeatablity Criteria Is Mol%] Renotability Accomplex.			000	000	0000	0000	0.00	-	8 8 8 8		+++		8 8 8 8	000	8 8 8 8	000	0.17 1.00 VES	0.17 1.00 VES
Process GC Analysis (Mot%) 11/10/2003 Max. Absolute Daviation (Mot%) Reproducibility Critaria (± Mot%)	11/10/2003	16.67	0.9018	0.26	7.033							-	0.00	0000	0.4246	088	1187.0873 2.50 3.00	1167.7178 2.45 3.00
Reproducibility Acceptable?			ON	YES	£8	\Box	SE)	60	\vdash	+	YES		SE XES	93	ĝ.	KES.	YES	YES
Sample HP2	Date	Sample Time		methans	ethana	propine is		utane			-	CD .	\rightarrow	-	200	ш	Hy dry (Blu/scf)	Hy set (Btu/sct)
Sample Bottle GC Analysis 2 (MoRS)	1010000	12	1.0226	84.519	$\overline{}$	4.0362	0.9443	1,0865	0.3632	-	-	\Box	0.0216		0.4907	00	1190.262	1170,8398
Bample Bottle GC Analysis-3 [Mof%] Max. Absolute Deviation-Successive [Mof%]			0.02	0.03		0.00		88		_	+		0.00		0.00	000	1190.0668	1170.5478
Max. Absolute Deviation-Overal [Mot%] Repeatability Critoria (± Mot%)			0.03	0.03	0.00	000	0.00	000	000	000	0.00	000	000	000	000	000	1.00	0.19
Repeatability Acceptable? Process GC Analysis (Motos)	110100003	15-51	YES	YES 84.8819	YES 7,039	\vdash	YES	\vdash	\vdash	\vdash	Н-	H	YES	\vdash	YES 0.4245	S -	YES 1187 0873	YES 1167,7178
Max. Absolute Deviation [Mot%]			0.13	036	700	99	0.02	_	\rightarrow	-	Н	H	000	\vdash	700	000	347	312
Reproducting Criteria (# Morta) Reproductating Acceptable?			2	YES	YES	X ESS	YES	+	₩	₩	++	\forall	YES	₩	YES	YES	NO NO	NO
Sample HP3		Sample Time		methane	ethane	auedo	so-butane n		pentane n-		+		-	10	200	\top	Hr dry (Blurisci)	Hr sat (Btu/sct)
Sample Dottle GC Analysts-1 [Morss] Sample Bottle GC Analysts-2 [Morss]	11710/2003	2		84.6395	_				13604		-	+	0.0219	+	0.4533	0	1190,9057	1171.4725
Sample Bottle GC Analysis 3 [Mot%]			0.913	84.6396	7.0038				0.3603		-	Н	97000	Н	0.4632	0	1190,9127	1171.4788
Max. Absolute Deviation-Successive [Mol%] Max. Absolute Deviation-Overall [Mol%]			800	500	88	000	88	800	800	88	800	88	88	88	88	800	888	000
Repeatability Criteria [± Mol%]			0.02	0.62	0.18	\rightarrow	Н		0.02		\rightarrow	Н	0.02	0.02	0.02	000	1.00	1.00
Repeatability Acceptable? Decrees GC Applicate Motion	11/10/00/0	18.01	NES D ROSE	VES 84 8736	7.0427	+	+		YES		+	+	YES	, ES	VES 0.4248	, E8	YES 1128	YES 1167 7534
Max. Absolute Daviation [MoDis]	11/10/2007	2	0.020	0.23	0.04	-			200		-		0.01	0.00	0.04	000	382	3.75
Reproducibility Criteria (± Mol%)			0.04	0.63	0.28	\rightarrow	Н		100		\rightarrow	\Box	0.04	0.04	0.04	100	300	3.00
Reproducibility Acceptable?			ZES.	ğ	ğ	2	ž	ZES	ZES.	2	ZES	22	ğ	ž.	ß	20	MO	MO
Sample HP4	Option	Sample Time	nitropan	methana	ethane	propare iso-butana		o-butane i-c	- pentane	anathan-n	havanes	haptanes	octanes	nonanes	8	22	Hv dry (Btursof)	Hv sat (Btu/scf)
Sample Bottle GC Analysis-1 [MotSc] 11/10/2003 16	11/10/2009	16.06 - 16.07			-						-	\vdash	-			П		
Sample Dottle GC Analyster 2 [MoTS] Eample Bottle GC Analyster 3 [MoTS] Max. Absolute Denation-Successive [MotS]																		
Max. Absolute Deviation-Overall (Not's) Repeatability Criteria (± Mot's)								\parallel	\parallel	\parallel	\parallel		\parallel					
Hepestability Acceptable? Process GC Analysis [MotSs]	11/10/2003	16.06	0.8924	84.8756	7.0449	++	++	-	0.3431	+	0.1275	+	7610.0		0.4247	08	1187 3406	1167.9868
Reproducibility Orderia ± Mol'55 Reproducibility Acceptable?			100	8 23	5 190	4 D	78.0	888	+++	700	0.04	700	700	35	104	88	3.00	3.00
See 1	ě									- 1					8		11	
Sample Mrs. Sample Bottle GC Analysis-1 [Moris]	11./10.2003	Sample Time 16:10 - 16:11	D.9456	B4.7939	-	3.5094 3.5094	e		0.3557	0.2403	-		-	+	775	Ş	1188.4007	1169.0094
Sample Hottle GC Analysis 2 Morts. Sample Bottle GC Analysis 3 Morts.			0.9564	84.7439	_	-	28480		524		+	+	+	-	0.4344		1168.742/	1168 5816
Max. Absolute Deviation-Successive [Mol/k.]			000	8	000	_	_		000		Н	Н	-	-	000	000	0.45	0.44
Max. Absolute Denation-Overall [MoTS.] Reveatchille Criteria I+ Motiful			88	9 6	8 8	+	_	+			+	$^{+}$	+	+	88	88	88	100
Repeatability Acceptable?			£	, SES	Z S S	H	\vdash	\sqcup	9		₩	H	+	₩	VES	VES.	XES .	SEX.
Process GC Analysis [Mot%] Max. Absolute Deviation [Mot%]	11/10/2009	18:10	0.8903	0.20	7,0802	3,9617	10.0	1.0471	03386		0.1249	0.0697	0.0181	0 80	0.426	08	1186,9443	1168.594
Reproducibility Criteria (± Mol%)			DO0	0.63	0.26	Н	\Box	Н.			Н	+	+	-	0.04	100	300	300
reproducting Acceptable			No.	150	100	100	021	Q II	Q III	100	9	150	100	100	011	9	120	JEG

Table D-6. Detailed results from Powder Wash sampling tests, November 10, 2003: High-Pressure Helium Displacement method.

Sample Bottle GC Analysis - [Marks] 11/10/2003 Sample Bottle GC Analysis - [Marks] 11/10/2003 Sample Bottle GC Analysis - [Marks] Max. Absolute Deviation-Successive [Math.] Recentable Deviation-David [Math.] Recentable Deviation-David [Math.]	11/10/2008	Sample Time 16:30 - 18:33	0.8944 0.8943 0.8945 0.00 0.00	methans 84.7343 84.7428 0.02 0.02 0.02	7.0323 7.0345 7.0374 0.00 0.18	3.953 3.953 3.953 0.01	0.9063 0.9063 0.9069 0.9069 0.00	1.0727 1.0727 1.0727 0.00 0.10	0.3765 0.3765 0.3768 0.000	0.2594 0.2594 0.2594 0.00 0.00	0.168 0.1683 0.000 0.000	0.1107 0.1107 0.1107 0.000 0.000	0.0311 0.0317 0.0317 0.011 0.011	0.0013 0.000 0.000 0.000	0.4369	NoooB 800	1193 2324 1193 2324 1192 7186 1193 0447 0.51 0.51	Hv sat [Btw/sc0] 1173.7803 1173.755 1173.675 0.51 0.51
Repeatabley Acceptable? Protess CC Analysis (Mo15) Max. Absolute Deviation (Mo15) Reproducibility Acceptable? Reproducibility Acceptable?	11/10/2003	16.34	0.886 0.086 7.65							YES 0.2159 0.04 NO	VES 0.1175 0.004	0.065 0.05 0.05 NO	7ES 0.0162 0.012 7ES		0.4636 0.4636 7ES	7ES 00 00 00 00 00 00 00 00 00 00 00 00 00	YES 1184.73 8.90 3.00	YES 1166.4001 8.36 3.00 NO
Sample ET2 Sample Buttle CC Analysis-1 [MotS2] Sample Buttle CC Analysis-2 [MotS2] Sample Buttle CC Analysis-2 [MotS2] Max. Absolute Deviation-Successive [Md/N] Max. Absolute Deviation-Deviation-Deviation-Buttle Successive [Md/N] Repeatablity Crisins is HAMN, Repeatablity Acceptable? Max. Absolute Deviation [MotS2] Max. Absolute Deviation [MotS2] Reproducibility Acceptable?	11/10/2003	Sample Time 16:37 - 16:38 16:38	nitrogen 0.0882 0.000 0.00 0.00 7ES 0.00 0.00 0.00 7ES 0.00 0.00	Mathana 84,775 84,7053 94,7053 001 001 052 YES 84,9675 0.38 0.38	9thans 7.0803 7.0803 0.00 0.00 0.18 VES VES 0.03 VES VES	9199me is 33962 3.9963 0.00 0.00 0.01 VES 0.013 VES VES	90-butann n 0 92774 0 9277 0 9276 0 0 0 0 0 0	neutrans 1.0732 1.0733 1.0733 1.0733 1.0733 1.0733 1.0745 1.0755	1-partition of 0.3884 0.3884 0.3887 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	0.2543 0.2543 0.2544 0.2544 0.00 0.00 0.00 0.01 0.014 0.014 0.014	Manage 0.1596 0.1601 0.000 0.000 0.000 0.000 0.004 0.004	Neganas 0.1047 0.1047 0.1051 0.00 0.00 0.02 YES 0.04 0.04	octanes 0.039 0.039 0.01 0.01 0.02 7.65 0.02 0.02 0.02 0.02	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	002 0.0440 0.0440 0.00 0.00 0.00 0.00 0.	# 0000 0000 0000 0000 0000 0000 0000 0	1192.732 1192.732 1193.336 1193.336 0.64 0.54 1.00 Y.ES 1184.0135 9.32 3.00 NO	H sel [Buve0] 1173-877 1173-877 1173-877 1173-877 1173-877 1100 1100 1100 1100 1100 1100 1100 1
Sample EF3 Sample Bottle CC Analysisc Mn PS Earthel Bottle CC Analysisc Mn PS Earthel Bottle CC Analysisc Mn PS Max. Absolute Deviation-Discussion Mn PS Max. Absolute Deviation-Deviation-Discussion Mn PS Repeatability Acceptable? Max. Absolute Deviation Mn PS Repeatability Acceptable? Max. Absolute Deviation Mn PS Max. Absolute Deviation Mn PS Reproducibility Acceptable?	Date 11/10/2008 11/10/2008	Sample Time 16:44 - 18:46 16:43	nitrogen 0.0814 0.0613 0.00 0.00 0.02 VEB 0.08 0.03 0.03	Methane 84,3968 84,3968 84,3962 0.01 0.01 0.62 VES 0.62 0.62	2,1357 7,1384 7,1384 0,00 0,00 0,16 7,0408 0,10 0,10 0,10 0,10 0,10	4.073 4.073 4.073 4.073 0.00 0.00 0.10 7ES 3.9674 0.11	0.08996 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	1,1223 1,1245 1,1245 1,1245 1,1245 1,000 0,10 7,EE 1,0244 1,0244 1,0244 1,0244 1,0244	1. Pentana 0.3973 0.3984 0.00 0.00 0.00 0.02 0.02 0.03 0.00 0.00	0.2714 0.2714 0.2723 0.000 0.00 0.02 VES 0.2161 0.06 0.06	0.1587 0.1587 0.1504 0.000 0.000 0.002 VES 0.0161 0.004	0.1039 0.1039 0.1046 0.00 0.00 0.00 0.02 VES 0.0646 0.04	0.00291 0.00291 0.00292 0.000 0.000 0.001 0.0178 0.0178 0.0178	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.02 0.4768 0.4768 0.4768 0.00 0.00 0.02 765 0.03 0.03 0.0434 0.044	7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1197-7978 11997-7978 1198-1067 0.20 0.31 1.00 YES 1183 8436 114.35 3.00 NO	Hr sat (Buvier) 1178-45 1178-45 1178-45 1178-45 1178-45 1100 VES 1100 VES 1104-5883 1102 300
Sample Et at 1 Morse 2	Data 11/10/2003 11/10/2003	Sample Time 16:50 - 16:52 16:52	nitrogen 0.0636 0.0636 0.00 0.00 7ES 0.02 0.02 0.02 0.02	methans 84,4207 84,308 0.02 0.03 VES 95,043 0.65 0.63	27.07.25 7.07.25 7.07.74 7.07.74 0.00 0.00 0.01 0.01 0.01 0.00 0.05 7.08885 7.0886 7.0886 7.0886 7.088	40437 40437 40433 40635 0011 010 7ES 339073 015	10.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	2.000 0.000	1-partana n 0.422 0.422 0.4237 0.00 0.00 7°ES 0.3264 0.10	P. pentians 0.296 0.296 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	Maranes 0.1965 0.1965 0.00 0.00 0.00 VES VES 0.117 0.00	Naptanas 0.1171 0.1181 0.00 0.00 0.02 YES 0.065 0.006	Octanes 0.0287 0.0289 0.011 0.012 VES 0.012 0.012 VES 0.0191 0.012	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.04654 0.4454 0.4453 0.04653 0.000 0.000 0.001 0.001 0.001	HO 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	He dry (Bluved) 1200 7421 1201 3578 1201 3547 0.63 0.63 0.63 1.00 1.00 1.00 3.00 0.00	Hw set (Bhu/set) His 1.441 His 1.7641 His 1.7641 0.62 0.62 0.62 1.00 YES His 3.608 3.00
Sample EES Sample Bottle GG Analysis [Not85] Sample Bottle GG Analysis [Not85] Sample Bottle GG Analysis [Not85] Mac. Absorble Dovision-Successive [Mol95] Mac. Absorble Dovision-Overal [Mol95] Repeatability Acceptable Mol95 Repeatability Acceptable Mol95 Mac. Absorble Dovision [Mol95] Mac. Absorble Dovision [Mol95] Reproducibility Acceptable Mol95 Reproducibility Criteria [Mol95] Reproducibility Criteria [Mol95] Reproducibility Criteria [Mol95] Reproducibility Acceptable Mol95	0ate 11/10/2003	Sample Time 16:57 - 16:59 16:56	natrogen 0.08545 0.08543 0.000 0.00 0.000 0.001 0.001	methane 84.9521 84.9521 0.01 0.02 VES 84.9519 0.63 VES	2,002 2,005 2,005 0,00 0,18 2,00 0,18 2,00 0,00 0,00 0,00 0,00 0,00 0,00 0,0	93981 4000 4001 000 010 010 010 010 013 VES	100 000 000 000 000 000 000 000 000 000	1,1022 1,1022 1,103 1,103 1,000 0,00 0,00 0,00 0,00 0	0.4017 0.4017 0.4017 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	0.2814 0.2815 0.2819 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	0.1772 0.1772 0.1789 0.00 0.00 0.00 0.00 0.0163 0.0163 0.004	heptanes 0.1151 0.1165 0.000 0.000 0.002 VES 0.0647 0.004 0.004	octanes 0.031 0.0318 0.00 0.00 0.00 0.00 0.00 0.0151 0.0151	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.4316 0.4316 0.4316 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	25000000000000000000000000000000000000	1197 2016 1197 2016 1197 2016 1197 2016 0.23 0.23 0.03 100 100 100 100 100 100 100 100 100 1	He sat [Bu/lec] 1177 5572 1177 5679 0.23 0.32 1.00 VES 1164 4571 1164 4571 3.00

Table D-7. Detailed results from Powder Wash sampling tests, November 10, 2003: Pitot and Bypass method.

Samuelo BB4	000	Google Too		mothono	-		o budgeon o	o buttone Le				н		H	8	77	des (Destroy)	the cost (Discover)
Sample Bottle GC Analysis-1 (Mot%)	11/10/2003 17:	17.31 - 17.32	1	84.9715	8.5186	3.5043	0.8943	$\overline{}$	0.3619	0.2509	+	0.0977	0.0163		34177	0	7908301	182
Sample Bottle GC Analysis-2 [MorSs]				81.6073	_			Н	382		1448	-	D3101	_	0.4088	0	1122.3856	1104.0797
Max. Absolute Designer-Successive Mod%!			2,68	100	622	3.37	0.87	+	+	+	0.14	$^{+}$	0.02	$^{+}$	0.41	000	1122.36	1104.08
May Absolute Designar-Darral Mores			2 12	5 70	1 0	5 6	98	+	+	t	1 11	t	100	t	191	800	1188 71	1149.75
Repeatability Criteria ± Mol%			0.10	0.62	0.18	10	0.02	Н	000	000	0.00	000	000	0.00	000	00	1.00	1.00
Repeatability Acceptable?		ŗ	00000	2000	2000	+	2	Ŧ.	2	Τ.	2000	†	YES	$^{+}$	2000	YES	NO MO	NO 0000
May Alcohde Deviction MidNSU	11/11/2003	0007	0.0900 4.79	84.9040	7 113	+	0.9041	-	+	+	2012	t	2000	Ť	0.4310	- 5	1104,0002	1100.174
Reproducibility Orbania (± Mol%)			100	0.63	920	0.13	10.0	0.13	н	Н	0.04	t	0.04	t	0.04	100	300	3.00
Reproducibility Acceptable?			QM MO	9	Q.	9	9	Н	Н	Н	Q.	Н	YES	Н	9	KES.	9	NO NO
A STATE OF THE STA		Ш			-						\rightarrow	-			8			
Sample PP2	-	Smill eldmes	_	_	+		o-pregna-o	- angula	Partian III	_	-	+		_	200	E .	Dosmacil	HV sat (btu/sct)
Sample Bottle GC Analysis 1 Morss Sample Bottle GC Analysis 2 Morss	11710/2003	82	0.8572	84.8614 84.8613	7001	3.9074	98180	1.0639	0.3801	0.2851	0.1885	0.1044	_		0.4279		1151 JOBO 174	1172.4403
Analysis			0.857	_	_		85160	1.0641	13802		-	+	$^{+}$	-	14283	0	1192.0856	1172,6325
Max. Absolute Deviation-Successive [Mol%]			000	_	-		0.0	000	000		\vdash	Н	П	_	80	000	0.18	0.17
Max. Absolute Deviation-Overal [Mor%]			800	_	_		8.8	800	000		-	-	\forall	_	88	800	019	0.19
Repeatable Create # Money			VES	_	+		VES	+	Т	_	+	+	+	-	AFS.	NES	YES	YES
Propess GC Analysis (Mot%)	11/10/2003	17.41	0.8739	_	+		0.9049	Ľ	I	_	+	+	$^{+}$	-	1.4487		1184.6845	1165,3651
Max. Absolute Deviation [Mot%]	-		0.02	_	_		10.0				-	Н		_	0.02	000	7.39	7.27
Reproducibility Criteria (± Mol%)			100	90	\rightarrow		0.04	+		_	-	+	\forall	_	100	0.04	300	3.00
Reproductority Acceptable?			Ž Ž	-	-		2	2	20	2	2	2		2	2	200	2	2
Sample PP3	Date	Sample Time		тефале	+		a-butane n		-u eutrane	_	vexanes	heptanes	-	nonanes	200	± SZH	dry (Btu/sct)	Hv sat (Bbu/sct)
Sample Bottle GC Analysis-1 [MoRS] 11/10/2008	11/10/2008	1747-1749		85.1878	-				3,3708	_	Н	Н	Н		3,4426	0	1186.4833	1168.1213
Sample Bottle GC Analysis-2 [Morss]			0.9005	B5.2072	_	_	_	-		_	-	+	7200		0.4434	0	1185.2027	1165.8651
Sample Dottle GC Analysis of Morse, Mark Absolute Detector Discount Discoun			0.9017	878	-	-	_	-		_	+	$^{+}$	0.0314	+	0.000	5 8	10407.0	1100.0408
Max. Absolute Deviation-Overall (MoTS)			000	900	-	-	_	-		_	+	$^{+}$	100	+	88	000	600	80
Represtability Criteria [± Mol%]			0.02	0.62	-	_		_		_	Н	Н	0.02	Н	0.02	0.02	1.00	1.00
Repeatability Acceptable?		Ш	YES	ΥES	\rightarrow	\rightarrow	П	\vdash		_	Н	Н	YES	Н	YES	YES	YES	YES
Process GC Analysis (Mot%)	11/10/2003	17-50	0.0686	84,9907	\rightarrow	_	$\overline{}$	-		_	-	+	2002	+	0,4449	0	1184825	1166.4834
Mac. Absolute Deviation (Notice) Recorducibility Criteria I+ Mol85)			3 2	800	-	9 65	т	0.13	30	300	+	100	300	880	300	300	300	98
Reproducibility Acceptable?			YES	2	, ES	-	$\overline{}$	-		-	YES	$^{+}$	£83	+	Ę Ę	YES	, see	, EB
Sample PP4	Date	Sample Time		methana	-	-	butana		ontana n-		Н		-	-	200		15	Hy sat (Blu/sct)
Sample Bottle GC Analysis 1 MotSc) 11710/2003 17	11/10/2009	17:56 - 17:58		84,9579	$\overline{}$	_	6927		0.382		-	-	\rightarrow		0.4256		1189.0774	1169,6747
Cample Dottle GC Analysis 2 (NOTS)			0,000	84.9441 DE 0417	_	-	0.080.0		5000		+	$^{+}$	-		U450V		1108.2432	1168.8378 116E.6177
Max. Absolute Deviation Successive Mol%			000	0.10	_	-	700		000		+	t	-	_	000		3.28	323
Max. Absolute Deviation-Overal [MoPS.]			000	0.10	-	0.03	Н		200		Н	Н	\rightarrow	ш	000		328	323
Repeatability Criteria (± Mol%)			000	0.62	\rightarrow	919	$^{+}$		200	- 1	+	$^{+}$	\rightarrow	_	201	- 1	1.00	1.00
Repressioning Acceptable? Process GC Analysis (MotS)	11/10/2003	17.55	0.8603	86 1213	7,0387	39176	150	1.0365	0.3508	323	0.1228	000	20131	3-	0.4278	20	1185.3275	1165.9874
Max. Absolute Deviation [Mot%]			100	0.08	-	0.01	Н		100		Н	Н	-	ш	000		3.82	3.85
Reproducibility Criteria (± Mol%)			MO10	E90	-	2013	+		A00	- 1	+	+	\rightarrow	_	100		3.00	3.00
Reproductority Acceptable?			Ž.	g	+	9	+		2		+	+	-	4-	0		2	2
1 0										11	Н	Ħ		н				П
Sample PPS Samela Bottle GC Analysis (19698)	Date 1 14 CID CID 3	Sample Time	natrogen n arrav	methane BS 3514	-	3.745B	n anton		- pentane n-	n-pertane h	+		n mana	10	2002	¥ -	dry (Bhu/sct)	threat (Dturbed)
Samele Bottle GC Analysis 2 (MotSS)	-		0.9018	95,350	_	3.7480	0.9027	1 030	13627		+	t	0.000	-	0.4336	0	11917191	1165 3898
Sample Bottle GC Analysis 3 [MotSc]			0.9047	95.2162	_	3.7806	0.9058	1.0389	3683		+	t	9000	-	3.4348	0	1186,5884	1168 2247
Max. Absolute Deviation-Successive [Mol%]			000	0.04	_	10.0	0.0	000	000	_	+	t	0.01	+	000	000	0.85	0.83
Max. Absolute Deviation-Overall [Mot%]			000	0.05	$\overline{}$	0.01			500		Н	Н	0.01	Н	80	000	980	0.83
Repeatability Criteria [± Mol%]			200	0.52	\rightarrow	99			201		+	\forall	0.02	+	201	200	1.00	1.00
Repeatability Acceptable?	44.40.0000	a a	YES	VES	$^{-}$	YES			VES C		+	YES	NES NES	+	YES	SE C	YES 440¢ 00¢s	YES 4400 £304
Max. Absolute Deviation IMpDM			0.002	0.29	_	0.16			2007	_	+	t	0.02	+	001	. 80	1.16	1.14
Reproducibility Criteria (± Mol%)			0.04	0.63	0.36	0.13		0.13	0.04		0.04	Н	0.04	0.04	10.0	0.04	3.00	3.00
Reproducibility Acceptable?			YES	YES	_	NO			YES		Н	Н	YES	Н	YES	YES	YES	YES

Table D-8. Detailed results from Powder Wash sampling tests, December 19, 2003: Fill-and-Empty method.

Sample FE1 Sample Bottle GC Analysis-1 [Marks] [12]	Date 8	Sample Time 13:57 - 14:09	nitrogen 0.7513	_	+	-84	9	9	9	a				\rightarrow	0.441	1	1210.6705	Hv sat (Btu/sct) 1190,9059
Sample Bottle GC Analysis-2 [MotSi] Sample Bottle GC Analysis-3 [MotSi]			0.7513	83,9954	72185	4.2859	1.025	1,1724	0.4486 0	2 K K K K K K K K K K K K K K K K K K K	0.2047	0.1101	0.0963	0.0005	0.4411	00	1210.7835 1210.7966	1191.0169
Max. Absolute Deviation-Successive [Mol%] Max. Absolute Deviation-Court [Mol%]			000	-	-	-	-	_	_	-	-	+	_	-	88	-	11.0	011
Repeatability Oritoria [# Mor8s]	\parallel		0.00		-	-	-	++	_	++	-	-	-	-	200	++	100	1.00
alysis [Morts.]	12/19/2003	14:02	7557.0	-	+	-	+		+	Н	+	+	+	-	14341	+	1210.B973	1191.1287
Max. Absolute Deviation [Mol%] Remoducibility Criteria I± Mol%]			000	-	_	_	-	_			-	_	_	-	000	+	300	300
Reproducibility Acceptable?			YES	-	\vdash	\vdash	н	\vdash	\vdash	Н	\vdash	+	\vdash	Н.	33	Н	YES	YES
Sample FE2	Date	Sample Time					o-butana n-		ontane 0-6	anatrae			_		005		w dry (Btu/scf)	Hv sat (Btu/scf)
5		14:10 - 14:15			-		1,0026		0.4017 0	97.73	\vdash	\vdash	-	-	0.433		1208.3388	1 1
Sample Bottle GC Analysis-2 (Mpt%)	T				_		1 0025		14017	1000	-	+	_	_	4331		1206.3522	
Max. Absolute Deviation-Successive [Mol%]	Ħ		$\overline{}$		-		0.00		0.00	000	\rightarrow	+	-	-	000		900	
Max. Absolute Deviation-Overal [MoTS] Reseatability Criteria (± MoTS)					_		0.00		000	8 6	-	_	_	_	0 0		000	
			П		\vdash		XES		XES	YES .	₩	H	-	ш	ž,	1 1	YES	1 1
Process GC Analysis [MoRS] 12 Max Absolute Decivior Didol%]	12/19/2003	14:13			_		10108		0.02	7167	-	_	_	_	0.4459		1207.2201	
Reproductability Criteria (# Mor%)	\parallel		0.04	189	0.26	E G	D 13	E1.0	0.04	700	1000	400	000	40 S	700	F 60 6	000	00 m
невтодоститу месералея					+ +		3		3	3	-	+	_	_	3		2	
Sample FE3		Sample Time	nitrogen		athana		so-butana n-	o-butana i-p	0		\Box	+	+	\rightarrow	202		Hydry (Blukser)	±
Sample Dottle GC Analysis 1 Mid % 12/	12/18/2003	1421 - 1420	0.7776	83 5005	_	4.4336	10101	_	0.409	0.2776	0.1824	0.1079	16800	9000	0.4294		1209.2702	188
Sample Bottle GC Analysis 3 [Mot95]			0.7774		-		1,0108	-	-	Н	Н	Н	_	-	0.4299		1209.2112	₽
Max. Absolute Deviation-Successive [Mol%]			000		-		000	-	_	_	-	Н	_	-	880		11.0	
Max. Adsolute Devation-Chefal (Notice) Repeatability Criteria [± MorSs]	T		8 6 6 6		-		8 00	-	_	+	+	+	_	-	888		1.00	
Repeatability Acceptable?			YES		\vdash		YES	\rightarrow	\vdash	Н	Н	Н	\vdash	₩	YES	II	YES	1 1
Process GC Analysis (Morss) 12/19/2003	2/19/2003	200	0.00		_		8660	-	_	+	+	+	_	-	0.4334		1205.2252	
Reproducibility Orteria [± MoPS.]	İ		500		_		200	-	_		+		_	-	200		3.00	
Reproducibility Acceptable?			YES		н		XES	-	+	Н	Н	Н	-	\vdash	YES	L. I	OM	
					-						-					- 1		
Sample F64 Committee Bottle OC Amelonical Industrial	Date 5	Sample Time	ntragen n 7,475	\rightarrow	+	_	OR .	-	_			+	-	-	C02			Hy sat (Btu/scf)
Sample Bottle GC Analysis-2 [Mot/s]	0000000	107	0.748	-	_	_	_	-	-	_	+	+	_	-	14286		$\overline{}$	1188.8314
Sample Bottle GC Analysis-3 [Mot%]			0.7474	\rightarrow	$\overline{}$	-	$\overline{}$	-	-	$\overline{}$	Н	Н	$\overline{}$	-	0.4283		П	1168,6963
Max. Absolute Deviation-Successive [Mol%] Max. Absolute Deviation-Deviation			88	-	_	_	_	_	_	_	+	+	_	-	88		\neg	900
Repeatability Criteria (± MoPS)	Ī		210	_	_	-	_	-	_	_	+	+	_	-	200			1.00
Repeatability Acceptable?			YES	\rightarrow	\vdash	-	-	\rightarrow	\rightarrow	\vdash	\vdash	H	\vdash	\rightarrow	YES	1 1	П	YES
Max. Absolute Deviation (Mol%)	WISVAUIIS	e e	0.003	-	_	_	_	-	_	_	+	+	_	-	000		\neg	210
Reproducibility Criteria [± MoTS.]			0.04	D.63	0.26	E	0.13	E1:0	0.04	700	0.04	NO.	0.04	8	0.04	NO.	300	300
Reproducibility Acceptable?			33	_	_	_	_	_	_	_			_	_	33			XES
Sample FE5		Sample Time	nitrogen	-	-		o-butana n-	-	- 0		\rightarrow	Н	-	-	C02		w dry (Bluksci)	Hv sat (Btu/sct)
Sample Bottle GC Analysis-1 [Mar95] 12		14:43 - 14:48	0.7524	_	-		1,0016	-			-	\vdash	-	_	0.4366		1209.452	1189,7077
Sample Bottle GC Analysie-2 [Mot%] Sample Bottle GC Analysie-3 [Mot%]	T	T	0.7523	_	_		1.0026	_			-	_	_	_	4266		1209.4603	1189.2158
Max. Absolute Deviation-Successive [Mol/k]			000		-		000	-	$\overline{}$		-	$\overline{}$	_	-	000		0.10	010
Max. Absolute Devation-Cheral (Noths) Repeatability Criteria [± MorSs]			8 23 0	_	_		36	_			-	_	_	_	8 28		0.00	201
Repeatability Acceptable?	CHOLON	17.1	YES	-	-		YES	-	$\overline{}$		\rightarrow	\vdash	_	\vdash	YES	1 1	YES	YES
Max. Absolute Deviation [Mot%]	MSVAUIS	14.46	000	0.14	0.05	900	0.01	100	0.01	000	000	000	000	000	0.00	- 8	2.47	243
Reproducibility Criteria [± Mot%]			0.04	_	-		0.04	-	$\overline{}$		-	+	-	ш.	0.04		300	-
Reproducibility Acceptable?			33	_	-		YES	_	\neg		_	\dashv	\neg	_	33	- 1	TES	- 1

Table D-9. Detailed results from Powder Wash sampling tests, December 19, 2003: Helium Pop method.

Sample HP1 Data Sample Bottle GC Analysis – [Mot95] 12/19/2003 Bample Bottle GC Analysis – [Mot95]	Data 12/19/2008	Sample Time 3 15:12 - 15:15	nitrogen 0.8212 0.8202	83.971 83.9735	7.1874 7.1877	4.4882 4.4882	1.0043 1.0039	1.1489 (1.1482 (0.3905 0.3904	0.2801 0.2801	0.1694 0.1595	0.1028 0.1029	0.0411 0.0413	0.0026 0.0026	0.4318	¥00	4v dry [Btu/scr] 1207.0873 1207.0808	Hv sat (Btu/scf) 1167.3827 1187.3753
Sample Bottle GC Analysis 3 [MoRS] Max. Absolute Deviation-Successive [Mol%]			0.8197	0.00	2,1887	0.00	_	_	-	_	-	0.1026	0.00	_	0.430	08	1207.1137	1187.4087
Mac. Absolute Deviation-Overal [Norse]			000	000	000	000	-	-	-	Н	Н	000	000	_	88	800	0.03	000
Repeatability Acceptable?			YES	YES	YES	YES	+	+	Н	Н	Н	YES	YES	+	YES	YES	YES	YES
inalysis [Mot96]	12/19/2009	15:16	0.7632	84.0296	72118	4.4845	-	-	-		-	0.1021	90000	_	0.4339	08	1207.1272	1187.4219
Reproducibility Orbania (± Mol%) Deproducibility Criteria (± Mol%)			200	0.65 0.65 0.65 0.65 0.65 0.65 0.65 0.65	0 S	0.13 E 85	-	-	Н.	Н	-	VES V	VES V	-	100 V	NES OF	3.00	300
Total de la contraction de la				3	3	3	-		-		+	3	3	1	3	3	3	3
	Opto	Sample Time	negozjiu	methane	П	-	programa	-		1.1	₩	hepternes	-	-	8	П	Hy dry (Blu/scf)	Hy sat (Btu/scf)
Sample Bottle GC Analysis-1 Marks	12/19/2008	15:18 - 15:19	0.9089	83,9023	$\overline{}$	_	-			_	-	0.106	_	-	0.4296	00	1206.5363	1186.8411
Sample Bottle GC Analysis-3 [Moriss]			0.9088	B3.8981	$\overline{}$	-	0042			-	-	0.1061	-	-	0.4298	- 8	1206.6208	1186.9242
Max. Absolute Deviation-Successive [Mot%] Max. Absolute Deviation-Overal [Mot%]			800	88	$\overline{}$	88	-			_	-	88	_	-	88	88	800	971
Repeatability Orbaria ± MolW			200	250	$\overline{}$	0.10	-			-	-	200	-	\rightarrow	200	00	1.00	1.00
nalysis (Mortis)	12/19/2003	1521	7ES 0.7818	84.8413	$\overline{}$	4,4617	+			+	+	21013	+	-	0.4316	200	1206.7762	1187.0768
			0.13	0.14	$\overline{}$	100	-			$\overline{}$	-	000	-	-	8	000	0.26	0.26
Reproductority Criteria (# M01%) Reproductority Acceptable?			NO	YES	YES	YES	VES VES	YES	YES	YES	VES	YES	YES	YES	YES	YES	YES	YES
		Sample Time	nitrogen	methane	ethane	н анкарта	so-butane	-houtane F	pentane n		Н	heptanes	\vdash	\rightarrow	88	H28	h dry (Blurisce)	Hr sat (Btu/sct)
Sample Bottle GC Analysis-1 (MotSs)	12/19/2008	1523 - 1526	0,7676	84.0378	7.1843	4,4875	7.0027	1,1622	0.3964	_	+	0.1042	_	-	0.4313	00	1207.808	1188.0913
Sample Bottle GC Analysis 3 Mot%			0.7672	84.0299	7.1839	4,4704	1,004	11683	0360	_	+	0.1049	_	-	0.4314	0	1208.0889	1168,3478
Max. Absolute Deviation-Successive [Mol%]			000	000	000	000	0.0	000	000	\vdash	Н	000	$\overline{}$	-	000	000	0.16	0.16
Max. Absolute Denatron-Overall (Mot%) Representability Coherin + Mot%)			800	000	8 5	8 5	8 5	8 9	888	_	-	888	_	_	88	88	989	989
Repeatability Acceptable?			YES	YES	YES	YES	YES	YES	YES	+	+	YES	+	-	YES	YES	YES	YES
Process GC Analysis [Mot55] 12/19/2003	12/19/2008	16.27	0.7641	84,0851	7,1817	4.4813	0.9963	1,1438	0.3884	\vdash	0.1879	0.1011	0.0384	21000	0.4304	0	1206.6497	1188,9624
Max. Absolute Deviation [MoP9] Description 2009. Creation L. MoHSO			000	900	980	500	500	500	500	_	+	000	_	-	88	88	2.6	9.5
Reproducibility Acceptable?			YES	YES	YES	YES	, ES	YES	YES	YES	+	YES	+	-	, ES	YES	YES	YES
Sample HP4	Date	Sample Time	negorge	methana	athana	s avedud	so-butana r	n-butane i-	- pentana n	n-pentane A	hasanea	haptanes	portenes	nonanas	88	E24	iv dry (Btu/scf)	Hy sat (Btu/scf)
Sample Dottle GC Analysis - Indoes	000000	800	0.7673	84.1551	7.0022		1 0048	1785		+	0.1737	0.1030	-	_	0.4288	0	1302 7429	1168 0272
Sample Bottle GC Analysis-3 [Mot%]			1757.0	84.1397	7.077		1.0052	1.1764		Н	0.1744	0.1049	$\overline{}$	_	0.4288	0	1207 5012	1188.2517
Max. Absolute Deviation-Successive [Mol%]			000	000	88		8.8	88		+	000	88	-	_	88	88	90	\$ 00 co
Repeatability Criteria ± Mol%			000	0.62	0.18		900	0.10		+	0.00	0.00	-	_	300	800	100	100
			YES	YES	YES		YES	YES		Н	YES	YES	\vdash	ш	ž.	YES	YES	YES
Process GC Analysis (MoRS)	12/19/2003	1532	0.7608	0.09	7.1594		0.9881	1.1453		_	0.1704	0.1012	-	_	0.4318	. 8	1206.8774	1187.1762
Reproducibility Orbania (± Mol%)			90	000	980		100	E1:0		+	0 B	700	-	_	104	88	3.00	3.00
Reproducibility Acceptable?			YES	SE .	<u> </u>		KES.	KES		\vdash	YES	SEJ.	-		ĘĘ,	YES	YES	YES
30H mlumn3	2	Summer Times	rajeos com	and de constant	1	1	hidana.	- Andrews		Н.	-	handana		1.	8	89	the other (Plansburg)	the and (Burland)
Sample Bottle GC Analysis-1 [MbRS]	12/19/2003	15:37 - 15:38	0.8751	84.009	7.146						-	9680'0	+		0.4382	20	1204.8445	함
Sample Bottle GC Analysis-2 [Mot95]			0.0755	B3 9994	7.1491	-	9941			-	-	96600	_	$\overline{}$	0.4382	0	1205.0036	1185.334
Mov. Alsohite Deletion, Successive MidNil			0.8749	84,0037	0.00	-	/786			+	-	0.00	+	_	0.4382	5 8	1204,5351	1108.17.13
Max. Absolute Deviation-Overal Mot%			000	000	88	-	+			+	-	888	+	_	88	000	017	0 0 0 0
Repeatability Criteria [± Mol%]			200	0.52	0.18	+	+			Н	-	200	+	\vdash	200	201	1.00	1.00
Repeatability Acceptable? Decrease Of Bostonic Model	12/10/20/20	16.38	VES	VES 44 004	7 1646	+	+			+	+	YES	+	+	VES	VES o	1306 G0034	YES 1187 0804
mioni more	in totalore	2000	1.12	600	0.01	100	0.00	100	000	000	100	0.00	000	000	000	. 8	2.15	212
Reproducibility Criteria (± Mol%)			00	0.63	0.38	+	+			+	\rightarrow	0.04	+	$^{+}$	004	809	300	300
Compared and the Proposition and the Compared and the Com						-	-			-	1				2	1		

Table D-10. Detailed results from Powder Wash sampling tests, December 19, 2003: Pitot and Bypass method.

Cample PD4	Doto		ognouse	mothana	۰	_	0	Authoria 11.	nantana	another.	banana	hantanaa	postorion	00000000	8	122	du des (Phistoch)	He eat (Brident)
Sample Bottle GC Analysis-1 [Mot95] 12/19/2003	12/19/2003	16.01 - 16.04	0.7818	84.1754	2,173	43466	0.9862	1,1214		0.2808	0.17	0.102	96600	0.0023	0.4408	0	1204,5869	1184,9242
Sample Bottle GC Analysis 2 [Morss]			0.7816	84.1722	_	_	_	-	_	0.7809	0.17	0.1023	96500	0.0024	0.4407	П	1204.6624	1184 9884
Mae, Absolute Desigtion-Successive (Mol%)			210/01	0000	_	_		-	_	000	0000	0.00	000	0.00	000	Т	0.08	000010
Max. Absolute Deviation-Overall [MoRS]			000	0.00	-	000	0.0	-	000	0.00	0.00	0.00	000	0.00	00		60.0	60.0
Repeatability Criteria [± Mol%]			000	0.62	\rightarrow	010	П	\rightarrow	\neg	0.02	0.00	0.02	0.02	0.02	000		1.00	1.00
Repeatability Acceptable? Decrease CC Apolices (Model)	12/18/2009	18.06	0.7300	87 1841	+	7 2965	Τ.	-	-	0.2840	0.4749	0 1041	1000	0,0010	0.4974	Т	1008.0749	1108 9808
Max. Absolute Daviation [MoRM]			900	0.01	_	000		-		0.00	0.00	0.00	000	0.00	000		1.49	1.45
Reproducibility Criteria (± Mol%)			104	0.63	Н	0.13	П	-	$\overline{}$	0.04	0.0	0.04	0.04	0.04	104	П	3.00	3.00
Reproducibility Acceptable?			ON	ĶES	_	<u> </u>	\neg	_	_	SS .	YES	χES	XES	£	ĘĘ	SE.	χES	YES
Cample BD2	Stoll	Same Time	ogroupo		-		o.bittono	opintano i	i contant		Powerpoo	horstone	outono	0000000	8		Hy dea (Phiritoce)	He cost (Bhuforfi
Sample Bottle GC Analysis: 1 Mor8:1	2	16:11 - 16:14	0.8003		+		0.9784	_		_	0.1691	0.1019	0.0399	0.0024	0.4404	T	1202,749	1183,1171
Sample Bottle GC Analysis 2 [MotSs]		-	8.0		-		-	_	$\overline{}$		0.1689	0.1026	0.0406	0.0027	0.4403	0	1209.0467	1183.4098
Sample Bottle GC Analysis 3 [Mot%]			0.7988		-		0.9814	$\overline{}$	_		0.1709	0.1036	00411	0.0027	0.4403	0 8	1203.3874	1183.7449
Max. Absolute Denatron-Successive [Mol%]			800		-	-	-	+	_	_	888	88	88	88	88	88	0.34	0.34
Max. Absolute Deviation-Overall (NOTS)			88		_	-	-	_	_	_	88	86	8 8	88	88	88	0.054	0.63
Recentability Acceptable?			YES		+	-	+	+	$\overline{}$	_	YES	YES.	YES.	, KES	9	YES	YES	YES
Process GC Analysis [Morts]	12/19/2003	16:10	0.7804		-	-	-	-		_	1.1691	0.1017	6800	0.0022	0.4399	0	1203.8474	1184.1971
Max. Absolute Deviation [Mot%]			0.02		-	\rightarrow	\rightarrow	_	$\overline{}$		000	000	000	000	80	000	0,1	1.08
Reproducibility Criteria # Morza Remoducibility Accentable?			VES	VES	4ES	VES	VES V	VES	VES	YES	VES	VES	VES	VES	VES	VES	XES YES	XIII
						-												
Sample PP3	Date	Sample Time		methane	ethane	propane in	so-butane n	-butane i-	pentane n	n-pertane	hexanes	heptanes	octanes	nonanes	200	Т	Hr dry (Blu/scf)	Hr sat (Btu/sct)
Sample Bottle GC Analysis-1 [MoRS] 12/19/2008	12/19/2008	16:22 - 16:24		84,3322	7,1539	-	_	+	+	0.261	0.1735	0.1047	0.0412	0.0026	0.4412	Т	1209,0663	1189,4199
Sample Bottle GC Analysis-2 [Morts.]				84.3259	7.1967	Н	+	Н	Н	1921	0.1726	0.1048	0.0412	97000	0.4413	0	1209.0997	1183.4519
Sample Bottle GC Analysis-3 [Mot%]			0.7529	84,3286	7,167	42652	90960	11041	0.3967	0.2811	0.1724	0.1045	0.0409	0.0027	0.4414	0	1209.0839	1183,4562
Max. Absolute Daviation-Successive (Mol%)			800	500	88	+	+	+	+	88	000	88	88	88	88	888	100	0.04
Department Colonia Letter (Moto)			888	500	3 5	+	+	+	+	88	888	888	88	88	38	88	180	100
Repeatability Acceptable?			YES	YES	YES	+	+	+	+	YES	YES	YES	YES	YES	YES	YES	YES	YES
Process GC Analysis [MoPS]	12/19/2009	18.21	0.79	84.3453	7.1389	Н	-	Н	Н	0.2548	0.1845	99600	0.0377	0.0023	0.4369	0	1201.2078	1181,6017
Max. Absolute Deviation [MoPM]			700	200	000	_	-	_	-	100	000	000	000	000	000	000	1.89	1.86
Reproducibility Criteria (± Mol78)			970	293	883	+	+	+	+	400	800	0.U4	#000 AE0	# OZA	\$000	970	900	300
Reproductority Acceptable?			Ę	ğ	ğ	_	-	-	+	2	2	2	ğ	ğ	ß	Ž.	ğ	3
Yamulo BB4	9000	Speeds Too	- 1	mothono	+		o buttone	_		T,	possesso	horstonen	portograp	00000000	8	Т	de des (Britania	
Sample Bottle GC Analysis 1 MotSci	5	1631 - 1633		84.4003	+		0.9067	-			0.1687	0.102	0.04	62000	0.4406	T	1201.3649	
Sample Bottle GC Analysis-2 [MotSc]		-		84,3962			0.9768	-		Н	0.1687	0.1021	0.04	0.0022	0.4406	П	1201.3913	
Sample Bottle GC Analysis 3 [Morts.]			0.7579	84,3959	+		0.9765	_		\pm	0.1687	0.1019	96500	00021	0.4408	Т	1201 3742	
Max. Absolute Deviation-Successive [Molth] Max. Absolute Deviation-Deviation.			800	880	-		38	_		+	880	88	88	88	88	Т	200	
Repeatability Criteria ± Mol%			000	0.62	-		0.02	-		Н	0.00	0.02	0.02	005	002		1.00	
Repeatability Acceptable?		Ш	YES	XES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	KES.	YES	YES	YES
More Absolute Decision (More)	12/19/2003	1632	0.04	84.4199	+		0.9727	_		+	0.1669	0000	00376	0002	0.4405	Т	1201.0583	
Remoducibility Criteria I± Mol%			100	0.63	+		0.04	-		+	8 8	0.04	0.04	0.04	104	Т	300	
Reproducibility Acceptable?			YES	ĶES	н		, LES	_		Н	YES	XES	XES	33	YES	П	YES	
Samula DDS	200	Samole Time		and the man				- hidana	o surprise		haven	hardana	portange		88	8	de des (Phuloce)	He east (Phinland)
Sample Bottle GC Analysis-1 (Mot%)	12/19/2003	1641 - 1643		84.5245	+	_	6	-	+	ь	0.1647	0.0968	0.0056		0.4374	300	1199.4834	1179.9061
Sample Bottle GC Analysis 2 (MotS)	==			84.5233	_	_	_	-	+	т	0.165	0.0974	0.0967		0.4373	0	1199.6214	1180.0418
Sample Bottle GC Analysis 3 [Mot95]			0,7349	84.5215	_	$\overline{}$		-			0.1647	696010	0.0959		0.4374	0	1199,5434	1179,9851
Max. Absolute Deviation-Successive [Mol%]			000	0.00	_	_	$\overline{}$	\rightarrow	Н	П	0.00	000	000		00	000	0.14	0.14
Max. Absolute Denation-Overall [MoSs]			88	86	_	_	_	-	+	т	88	88	88		88	88	100	1014
Repeatablity Acceptable?			YES	, SE	+	$\overline{}$	-	+-	+	Т	VES .	VES	VES		YES	VES.	VES	VES
Process GC Analysis [Mot96]	12/19/2009	16:43	0.7576	84.5025	-	$\overline{}$	-	-	Н		0.1622	0.0962	0.0968		0.4381	0	1199,0612	1179.4812
Max. Absolute Deviation [MoPM]			000	000	_	_	_	-	+	т	000	000	000		88	800	0.57	980
Reproducibility Acceptable?			YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES